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## **NORMAL D-REGION MODELS FOR WEAPON EFFECTS CODE**

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## SUMMARY

This report examines D-region models that are widely used to predict the performance of military communication systems. Four types of models, selected for this study, are described in Section 2. These are models based, respectively, on measured electron concentration profiles, physical representation of normal ion production sources and associated atmospheric chemistry models, inferences from VLF/LF propagation data, and prediction of the D-region absorption of electromagnetic waves in the HF band.

Results produced by the various model approaches are in reasonable agreement for the daytime D-region. Model adjustments to produce agreement among the results for daytime conditions can be easily made within allowable limits of parameter uncertainties of any of the models. Results produced for the nighttime D-region are not in good agreement. In general models based on electron concentration measurements, and those based on production rate and chemistry predict higher electron concentration in the 75 to 90 km altitude range than do those inferred from VLF/LF propagation measurements.

In Section 3, the rationale for adjusting profiles to match propagation data are discussed and parameter adjustments to produce profiles similar to those inferred from the VLF/LF propagation data are examined. A numerical procedure is defined for selection of normal profiles to provide for smooth transition from the selected normal to a disturbed profile. This procedure is applicable to simple models which use fixed reaction rates and assume a quasi-equilibrium solution to the deionization equations. The sensitivity of nighttime D-region profiles to variations in ion production rates and atmospheric reaction rates in more complex chemistry models is also examined. This sensitivity analysis indicates that the adjustments to reduce electron concentration cannot be obtained with changes in production rates and identifies the required changes in effective lumped-parameter chemistry reaction rates that would be required to match profiles inferred from propagation data. The required changes appear to be within allowable model limits. However, consistent changes in atmospheric constituents associated with the change in reaction

rates may have model implications for other systems or applications. The methods of implementing changes in the chemistry models are not defined.

The emphasis in Section 3 is placed on noon and midnight profiles. An important problem not addressed is day/night transition. The transition problem is another example where apparent discrepancies exist between empirical models and models inferred from propagation data. The empirical models show a very gradual transition. Propagation models show more abrupt transition. This is indicated by modal interference and signal phase variations measured as the day-night terminator moves along a propagation path.



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# CONVERSION TABLE

Conversion factors for U.S. Customary to metric (SI) units of measurement.

MULTIPLY  $\longrightarrow$  BY  $\longrightarrow$  TO GET  
TO GET  $\longleftarrow$  BY  $\longleftarrow$  DIVIDE

angstrom	1.000 000 X E -10	meters (m)
atmosphere (normal)	1.013 25 X E +2	kilo pascal (kPa)
bar	1.000 000 X E +2	kilo pascal (kPa)
barn	1.000 000 X E -28	meter <sup>2</sup> (m <sup>2</sup> )
British thermal unit (thermochemical)	1.054 350 X E +3	joule (J)
calorie (thermochemical)	4.184 000	joule (J)
cal (thermochemical)/cm <sup>2</sup>	4.184 000 X E -2	mega joule/m <sup>2</sup> (MJ/m <sup>2</sup> )
curie	3.700 000 X E +1	giga becquerel (GBq)*
degree (angle)	1.745 329 X E -2	radian (rad)
degree Fahrenheit	$t = (t^{\circ}f + 459.67) / 1.8$	degree kelvin (K)
electron volt	1.602 19 X E -19	joule (J)
erg	1.000 000 X E -7	joule (J)
erg/second	1.000 000 X E -7	watt (W)
foot	3.048 000 X E -1	meter (m)
foot-pound-force	1.355 818	joule (J)
gallon (U.S. liquid)	3.785 412 X E -3	meter <sup>3</sup> (m <sup>3</sup> )
inch	2.540 000 X E -2	meter (m)
jerk	1.000 000 X E +9	joule (J)
joule/kilogram (J/kg) (radiation dose absorbed)	1.000 000	Gray (Gy)**
kilotons	4.183	terajoules
kip (1000 lbf)	4.448 222 X E +3	newton (N)
kip/inch <sup>2</sup> (ksi)	6.894 757 X E +3	kilo pascal (kPa)
ktap	1.000 000 X E +2	newton-second/m <sup>2</sup> (N-s/m <sup>2</sup> )
micron	1.000 000 X E -6	meter (m)
mil	2.540 000 X E -5	meter (m)
mile (international)	1.609 344 X E +3	meter (m)
ounce	2.834 952 X E -2	kilogram (kg)
pound-force (lbf avoirdupois)	4.448 222	newton (N)
pound-force inch	1.129 848 X E -1	newton-meter (N-m)
pound-force/inch	1.751 268 X E +2	newton/meter (N/m)
pound-force/foot <sup>2</sup>	4.788 026 X E -2	kilo pascal (kPa)
pound-force/inch <sup>2</sup> (psi)	6.894 757	kilo pascal (kPa)
pound-mass (lbm avoirdupois)	4.535 924 X E -1	kilogram (kg)
pound-mass-foot <sup>2</sup> (moment of inertia)	4.214 011 X E -2	kilogram-meter <sup>2</sup> (kg-m <sup>2</sup> )
pound-mass/foot <sup>3</sup>	1.601 846 X E +1	kilogram/meter <sup>3</sup> (kg/m <sup>3</sup> )
rad (radiation dose absorbed)	1.000 000 X E -2	Gray (Gy)**
roentgen	2.579 760 X E -4	coulomb/kilogram (C/kg)
shake	1.000 000 X E -8	second (s)
slug	1.459 390 X E +1	kilogram (kg)
torr (mm Hg, 0°C)	1.333 22 X E -1	kilo pascal (kPa)

\* The becquerel (Bq) is the SI unit of radioactivity; 1 Bq = 1 event/s.

\*\*The Gray (Gy) is the SI unit of absorbed radiation.

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## SECTION 1

### INTRODUCTION

The D region, in the context of this report, includes the altitude range from about 40 to 100 km altitude. There are many applications for models of electron density in the undisturbed D region and as many models as there are applications. For computer codes that predict the effects of nuclear disturbance on the propagation of electromagnetic signals, the normal models provide the departure conditions and eventual recovery conditions of the ionosphere. While the nuclear effects models are not intended to be used for undisturbed predictions, reasonable models are required to provide for predictions of effects of weak disturbances and for estimates of recovery times. In addition, the nuclear effects codes suffer from a decrease in credibility when field strength predictions for non-disturbed or recovery conditions disagree with observed propagation data. Current normal ionosphere models in nuclear effects codes produce propagation losses larger than inferred from measured data. This discrepancy provided the impetus for this effort.

In this report, widely used models are discussed, showing similarities and differences and illustrating sometimes conflicting model requirements for obtaining generally applicable models for nuclear effect predictions. A numerical model approach is described that can provide some flexibility in a choice of normal ionosphere models. This revised model can be implemented in the SIMBAL code (Reference 1) for VLF and LF predictions. Implementation in models with complex chemistry calculations (such as WEDCOM, Reference 2) is discussed but the procedure is much more difficult.

Four types of models will be discussed. These are:

1. Hypothetical models which can be numerically specified and which can be used to reproduce detailed VLF and LF propagation data.
2. Empirical models derived from direct measurement of electron and ion density profiles.
3. Physical models based on models of normal ion-pair production sources and atmospheric chemistry models. This type of model is required for

nuclear effects codes, since the weapon-produced disturbances are modelled as additional ion-pair production sources and, in some cases, the disturbance changes atmospheric constituents and reaction rates.

4. Empirical models that reproduce observed values of D-region absorption of EM waves in the HF band.

In general, defining D-region models to reproduce VLF and LF propagation data is more difficult than defining models to reproduce HF absorption. VLF and LF reflection from the ionosphere depends on both the electron (and sometime heavy ion) concentration and vertical gradient. HF absorption is an integration of losses through the D region and can be reproduced by various vertical profiles. Both electrons and heavy ions can be important for VLF and LF, although ions usually have little effect for undisturbed conditions. In this report the D region will be characterized by electrons  $N_e(h)$ , representative positive and negative ions  $N_+(h)$  and  $N_-(h)$ , electron-neutral collision frequency  $\nu_e(h)$  and average ion-neutral collision frequency  $\nu_i(h)$ .

Table 1 lists collision frequencies that have been used in this report.

The important altitude band where the D-region electron concentration and gradient are important for VLF/LF reflection has been addressed by several researchers. The reflecting region is defined in terms of the square of the index of refraction,  $n^2$ , where

$$n^2 = 1 - A(h) - jB(h) \quad (1)$$

$$j = \sqrt{-1}$$

$$A(h) = A_e(h) + A_i(h)$$

$$B(h) = B_e(h) + B_i(h)$$

$$A_e(h) = \frac{3.18 \times 10^4 N_e(h) (\omega \pm \omega_{me})}{\omega \left[ (\omega \pm \omega_{me})^2 + \nu_i^2(h) \right]}$$

Table 1. Electron-neutral and ion-neutral collision frequencies.

Altitude (km)	Electron-Neutral Collision Frequency ( $\nu_e$ ) s <sup>-1</sup>	Ion-Neutral Collision Frequency ( $\nu_i$ ) s <sup>-1</sup>
5	8.08E+10	3.37E+09
10	3.97E+10	1.75E+09
15	1.82E+10	8.30E+08
20	8.22E+09	3.75E+08
25	3.74E+09	1.69E+08
30	1.73E+09	7.72E+07
35	8.19E+08	3.57E+07
40	4.05E+08	1.72E+07
45	2.08E+08	8.60E+06
50	1.10E+08	4.50E+06
55	5.86E+07	2.77E+06
60	3.05E+07	1.69E+06
65	1.54E+07	1.01E+06
70	7.52E+06	5.79E+05
75	3.53E+06	3.21E+05
80	1.58E+06	1.70E+05
85	6.82E+05	8.58E+04
90	2.91E+05	4.19E+04
95	1.27E+05	2.06E+04
100	5.75E+04	1.06E+04

$$A_i(h) = \frac{5.45 \times 10^4 N_i(h)}{\omega^2 + \nu_i^2(h)}$$

$$B_e(h) = \frac{\nu_e(h)}{\omega \pm \omega_{me}} A_e(h)$$

$$B_i(h) = \frac{\nu_i(h)}{\omega} A_i(h)$$

where

$\omega_{me}$  is the electron gyrofrequency.

Field and Engel (Reference 3) showed that when  $B(h) \gg A(h)$  reflection maximizes at  $h_r$ , where  $h_r$  is defined by

$$B(h_r) = \sqrt{2} \cos^2 \phi_i \quad (2)$$

and

$\phi_i$  = real angle of incidence.

Booker, Fejer, and Lee (Reference 4) extended the analysis to include variations in both  $A(h)$  and  $B(h)$  and defined the altitude  $h_r$  to be where

$$m(h_r) = \cos^2 \phi_i \quad (3)$$

In Equation 3

$$m(h) = \frac{2 M(h)}{(8 + \cos^2 \psi_i)^{1/2} - \cos \psi_i} \quad (4)$$

$$M(h) = [A^2(h) + B^2(h)]^{1/2} \quad (5)$$

and

$$\psi_i = \tan^{-1} (B(h)/A(h)) \quad . \quad (6)$$

Note that Equation 3 reduces to Equation 2 when  $B(h) \gg A(h)$ .

Figure 1a shows the electron concentration as a function of altitude that satisfies Equation 3 for frequencies of 20 and 100 kHz and  $\phi_i = 80$  degrees. Values are shown with and without the effects of the magnetic field. The approximate formulas are not strictly valid when magnetic field effects are strong. These curves can be used to approximate the altitude range where D-region profiles must match prescribed profiles to match propagation data.

Figure 1b shows the concentration of ions required to satisfy Equation 3 for the same conditions.

Numerical calculations (Reference 5) which evaluated the altitude variation of the magnitude of downcoming waves reflected from various ionospheres tended to verify Equations 2 through 5. The reflecting region is thin and well defined when the vertical gradient of the electron concentration is large. When the gradient is small, the reflection region is thick and the numerical results indicated that reflections come from a somewhat lower altitude than Equations 2 or 3 predict.

Numerical evaluation of the reflection region for selected specific profiles is presented in Section 3.



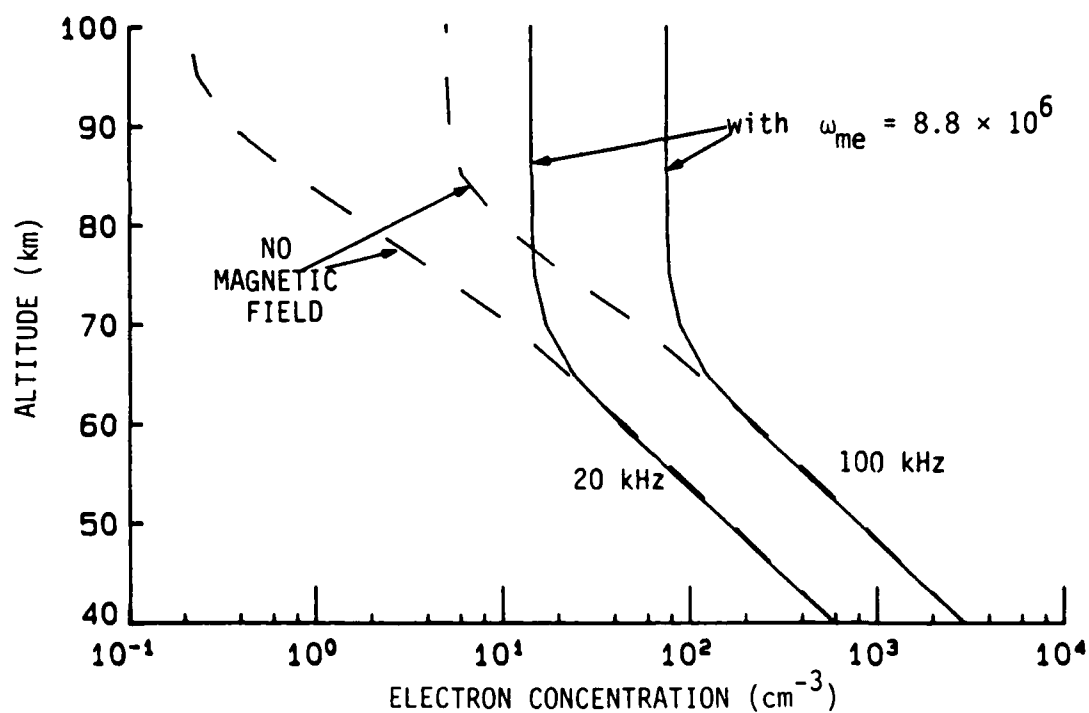


Figure 1a. Electron concentration to produce significant reflection for 20 and 100 kHz.

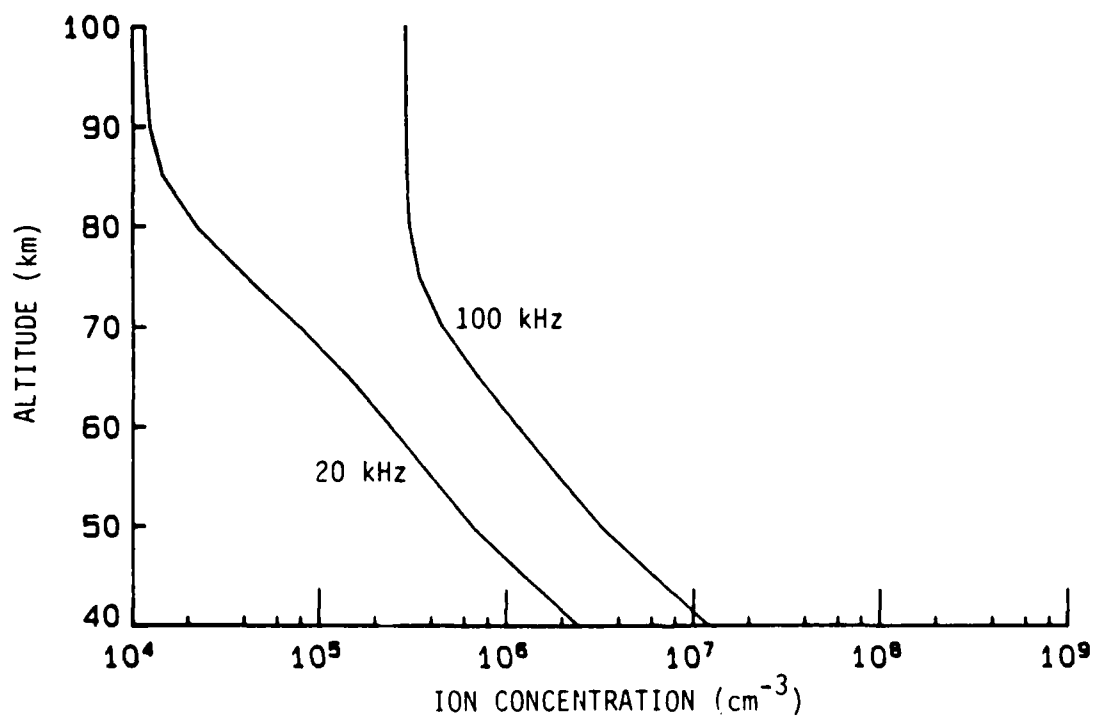


Figure 1b. Ion concentration to produce significant reflection for 20 and 100 kHz.

## SECTION 2

### WIDELY USED D-REGION MODELS

This report considers D-region models that are currently used widely in predictions of the performance of military systems in a disturbed environment. It is not intended to be a tutorial review of models. Four different types of models are discussed.

#### 2.1 PROFILES TO MATCH VLF/LF PROPAGATION DATA.

Morfitt (Reference 6) and others have performed extensive comparisons of measured VLF/LF field strength values with detailed predictions. The procedure is to assume an electron concentration profile of the form

$$N_e(h) = 1.43 \times 10^7 \exp(-\beta h_w) \exp((\beta - 0.15)h) \quad (6)$$

and perform calculation for various values of  $h_w$  and  $\beta$ . For selected  $h_w$  and  $\beta$  the computed and measured field strength values (measured field strength as a function of distance between the transmitter and receiver) show remarkable agreement, including the location of peaks and nulls produced by constructive and destructive mode interference.

Tables 2, 3, and 4 from Reference 6 show values of  $\beta$  and  $h_w$  that produce a best fit to measured data for several frequencies and for daytime and nighttime conditions. The implied frequency dependence of the ionosphere cannot be real. The changes with frequency may occur because the altitude of maximum reflection moves upward with increasing frequency, thus waves of different frequencies are affected by different segments of the ionosphere profile. Selected profiles ( $\beta = 0.3$ ,  $h_w = 72$  for daytime and  $\beta = 0.7$ ,  $h_w = 88$  for nighttime) are used for reference and comparisons in later subsections.

Table 2. Effective electron density profiles for use in propagation predictions, midlatitude - Pacific.  
(Source: Reference 6)

<u>Daytime</u>		<u>Nighttime</u>	
<u>Frequency</u>	<u>Profile</u>	<u>Frequency</u>	<u>Profile</u>
(kHz)	$\beta$ ( $\text{km}^{-1}$ ), $h_w$ (km)	(kHz)	$\beta$ ( $\text{km}^{-1}$ ), $h_w$ (km)
<u>Winter</u>		<u>Winter</u>	
9 - 60	$\beta = 0.3$ , $h_w = 74$	below 10	$\beta = 0.3$ , $h_w = 87$
		10 - 15	$\beta = 0.4$ , $h_w = 87$
		15 - 25	$\beta = 0.5$ , $h_w = 87$
		25 - 30	$\beta = 0.6$ , $h_w = 88$
		30 - 40	$\beta = 0.7$ , $h_w = 88$
		40 - 60	$\beta = 0.8$ , $h_w = 88$
<u>Summer</u>			
16 - 26	$\beta = 0.5$ , $h_w = 70$		

Table 3. Best-fit exponential electron density profiles - nighttime winter data recorded aboard an aircraft, Hawaii to Southern California propagation path. (Source: Reference 6).

<u>Hawaii Transmitter</u>							
<u>7 February 1969</u>			<u>30 January 1974</u>			<u>1 February 1974</u>	
<u>kHz</u>	<u><math>\beta</math> (<math>\text{km}^{-1}</math>)</u>	<u><math>h_w</math> (km)</u>	<u>kHz</u>	<u><math>\beta</math> (<math>\text{km}^{-1}</math>)</u>	<u><math>h_w</math> (km)</u>	<u><math>\beta</math> (<math>\text{km}^{-1}</math>)</u>	<u><math>h_w</math> (km)</u>
9.340	0.35	87	9.340	0.3	87	0.3	89
10.897	0.4	87	10.897	0.4	87	0.3	89
14.010	0.5	87	15.567	0.5	86	0.4	88
15.567	0.5	87	21.794	0.7	87	0.5	88
17.124	0.5	87	28.020	1.0	88	0.5	89
21.794	0.5	88	37.361	1.0	88	0.6	88
24.908	0.5	88	40.475	1.2	88	0.6	88
26.464	0.5	88	46.702	1.2	88	0.7	88
28.020	0.5	88	52.929	1.2	88	0.7	88
31.134	0.6	88	56.042	1.2	88	0.7	88

Table 4. Best-fit exponential electron density profiles -- daytime winter data recorded aboard an aircraft, Hawaii to Southern California propagation path. (Source: Reference 6).

<u>Hawaii Transmitter</u>					<u>Sentinel Transmitter</u>		
kHz	2 February 1974		2 February 1974		kHz	2 February 1974	
	$\beta$ (km <sup>-1</sup> )	$h_w$ (km)	$\beta$ (km <sup>-1</sup> )	$h_w$ (km)		$\beta$ (km <sup>-1</sup> )	$h_w$ (km)
9.340	0.3	72	0.3	75	9.336	0.3	74
10.897	0.3	72	0.3	75	14.003	0.3	74
15.567	0.3	72	0.3	75	17.115	0.3	74
21.794	0.3	72	0.3	75	24.895	0.3	74
28.020	0.3	73	0.3	75	28.007	0.3	74
37.361	0.35	73	0.3	75	34.231	0.3	74
40.475	0.35	73	0.3	75	38.898	0.3	74
46.702	0.35	73	0.3	75	43.566	0.3	74
52.929	0.35	73	0.3	75	49.790	0.3	75
56.042	0.35	73	0.3	75	56.104	0.3	75

## 2.2 MODELS BASED ON MEASUREMENTS OF ELECTRON DENSITY PROFILES.

### 2.2.1 Berry's Model.

Berry (Reference 7) analyzed a large number of experimentally determined vertical electron profiles and sought a model that would be useful for VLF and LF predictions. Following the lead of Morfitt and others at NOSC (Reference 6), who match propagation data using electron profiles with an exponential altitude variation, Berry also devised a model of the form

$$N(h_w) = N_o \exp -\beta(h_w - h_r) \quad (7)$$

where  $\beta$  is chosen to fit the slope of measured data at the altitude  $h_r$ , and  $h_r$  is the altitude where Equation 2 is satisfied, using a frequency of 30 kHz and an angle of incidence of 81°.  $N_o$  is defined to make  $h_w$  and  $\beta$  consistent with the entries in Tables 2, 3, and 4.

The parameters used in the fit were

- $X_1 = \cos \chi$  ( $\chi$  is the solar zenith angle)
- $X_2 = \cos \theta$  ( $\theta$  is the geographic latitude)
- $X_3 = \cos \phi$  ( $\phi = (m - 0.5)/12 \times 2\pi$ ,  $m$  = month)
- $X_4 = \text{SSN}$  (SSN is the smoothed Zurich sunspot number)
- $X_5 = \text{absorption index}$  (0 for quiet conditions,  
1 for disturbed conditions).

The equations for the parameters are

$$h_w = 71.81 - 7.84X_1 + 8.04X_2 - 1.23X_3 - 0.0371X_4 - 7.03X_5 \quad (8)$$

$$\beta = 0.353 - 0.120X_1 + 0.072X_3 + 0.171X_5 \quad (9)$$

Table 5 shows values of  $\beta$  and  $h_w$  for a latitude of 40 degrees, and various seasons, sunspot numbers, and times. Examples of Berry's results integrated with a physical model of the ionosphere are also shown in the next subsection. It can be seen that the nighttime reference altitudes are usually lower than the reference altitude used to match propagation data (Tables 2, 3, and 4). This may in part reflect the difficulty of making electron concentration measurements at the low concentrations that are important for VLF/LF propagation in the 75 to 85 km altitude range at night.

Table 5. Examples of altitude and slope parameters from Berry's model (quiet conditions).

Season	Local Time	SSN	$h_w$	$\beta$	$h_r$
Summer (July)	1200	10	71.2	.31	59.6
		100	67.9	.31	56.2
	0000	10	82.2	.48	74.7
		100	78.9	.48	71.1
Winter (January)	1200	10	72.9	.23	57.1
		100	69.6	.23	53.8
	0000	10	83.8	.40	74.7
		100	80.5	.40	71.5

### 2.2.2 McNamara's Model.

McNamara (Reference 8) extended the sets of profiles examined by Berry (Reference 7) and developed a numerical model of the electron density at heights of 55 to 90 km in 5-km steps. The model form is

$$\begin{aligned} \log_{10}(N_e) = & a + b \cdot x(\text{zenith angle}) + c \cdot x(\text{latitude}) \\ & + d \cdot x(\text{solar activity}) + e \cdot x(\text{season}) \\ & + f \cdot x(\text{magnetic index}) \end{aligned} \quad (10)$$

where  $a, b, c, d, e,$  and  $f$  are constants derived for the fit and the  $x$ 's provide the functional dependence on the independent variables. McNamara experimented statistically with different functional forms. The forms used to derive values for the constants are:

$$x(\text{zenith angle}, \psi) = \cos \psi ,$$

$$\begin{aligned} x(\text{latitude}, \theta) &= \sin 2\theta , & h \geq 75 \text{ km} \\ &= 0. + 0.9 \sin^4 \theta , & h \leq 70 \text{ km} , \end{aligned}$$

$$\begin{aligned} x(\text{solar activity, SSN}) &= 0 \text{ for low sunspot number (used here);} \\ &\text{otherwise not clear in Reference 8.} \end{aligned}$$

where

SSN = smoothed Zurich sunspot number

$$x(\text{season}) = \cos \left\{ \frac{m - 0.5}{12} 2\pi \right\}$$

where

$m$  = month, and

$$\begin{aligned} x(\text{magnetic index}) &= 0, \text{ quiet conditions} \\ &= 1, \text{ disturbed conditions.} \end{aligned}$$

Tables 6 and 7 show the constants generated by McNamara to fit over 700 profiles, and Figures 2 and 3 show the electron concentration profiles for mid-latitude, magnetically-quiet conditions. Winter and summer conditions are plotted for two-hour intervals from midnight to noon. Selected reference exponential profiles ( $\beta = 0.7, h_w = 88$  for night and  $\beta = 0.3, h_w = 72$  for day)

Table 6. The coefficients of the regression equation at heights from 55 to 90 km for magnetically quiet days (from Reference 8).

<u>Height (km)</u>	<u>Constant</u>	<u>Zenith Angle</u>	<u>Latitude</u>	<u>Solar Activity</u>	<u>Season</u>
90	3.21	0.80	0	0	0.15
85	2.32	0.86	0.23	0.13	0.16
80	1.87	1.03	0.16	0.20	0.17
75	1.64	1.00	0.09	0.25	0
70	1.49	0.86	0.17	0.13	-0.05
65	1.25	0.57	0.58	0.26	0
60	0.81	0.66	0.78	0.26	0.12
55	0.82	0.77	0	0	0

Table 7. The coefficients of the regression equation at heights from 55 to 90 km for all magnetic conditions (from Reference 8).

<u>Height (km)</u>	<u>Constant</u>	<u>Zenith Angle</u>	<u>Latitude</u>	<u>Solar Activity</u>	<u>Season</u>	<u>Magnetic Effect Term</u>
90	3.12	0.82	0	0.15	0.17	0.17
85	2.30	0.86	0.24	0.15	0.18	0.34
80	1.88	0.98	0.15	0.22	0.18	0.31
75	1.66	0.95	0.09	0.26	0	0.32
70	1.49	0.84	0.18	0.13	-0.06	0.32
65	1.25	0.58	0.57	0.26	0	0.21
60	0.81	0.68	0.78	0.25	0.12	0.45
55	0.82	0.77	0	0	0	0

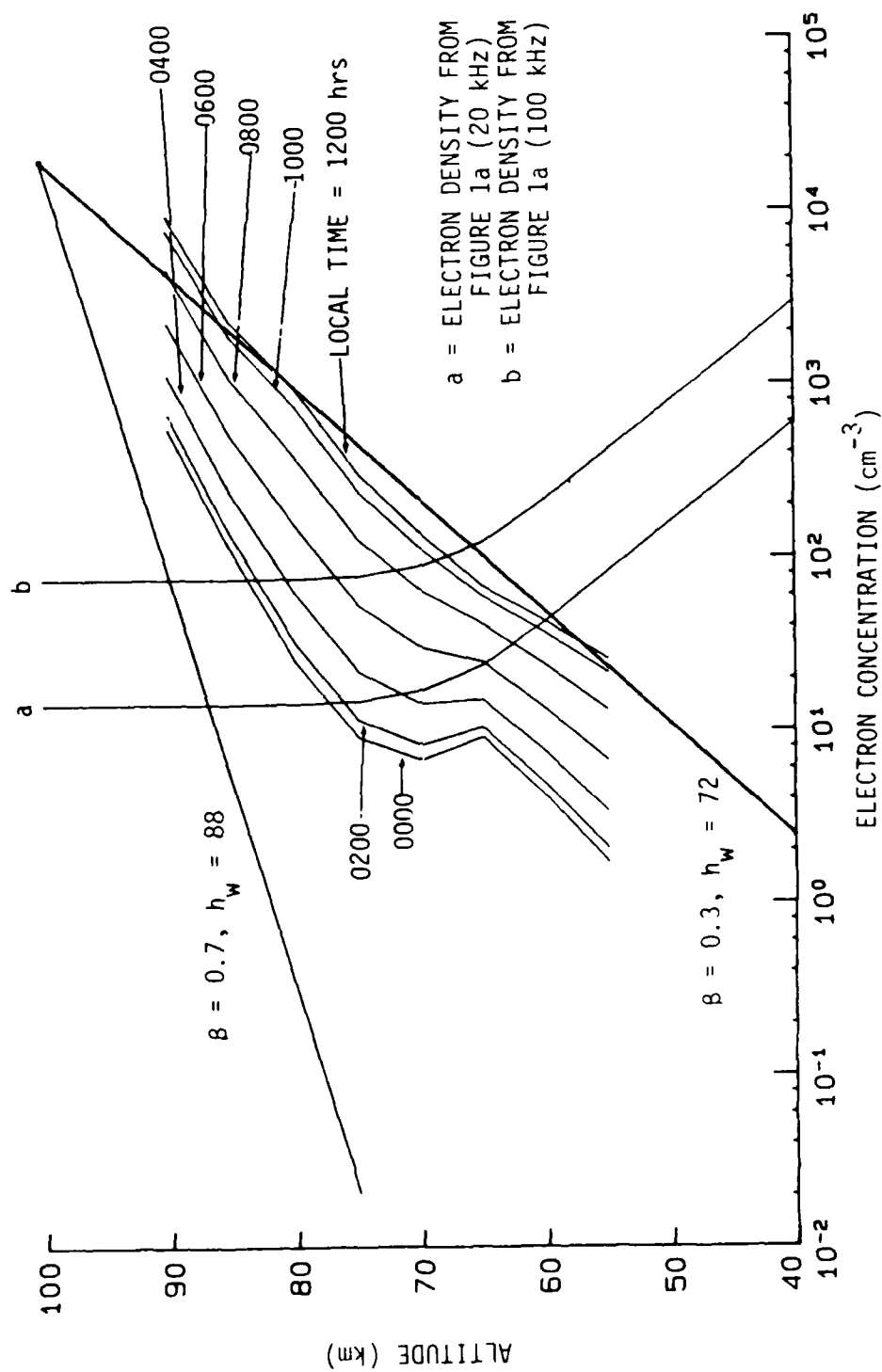


Figure 2. Electron concentration from McNamara's model (summer, magnetically quiet, low sunspot number, midlatitude conditions).



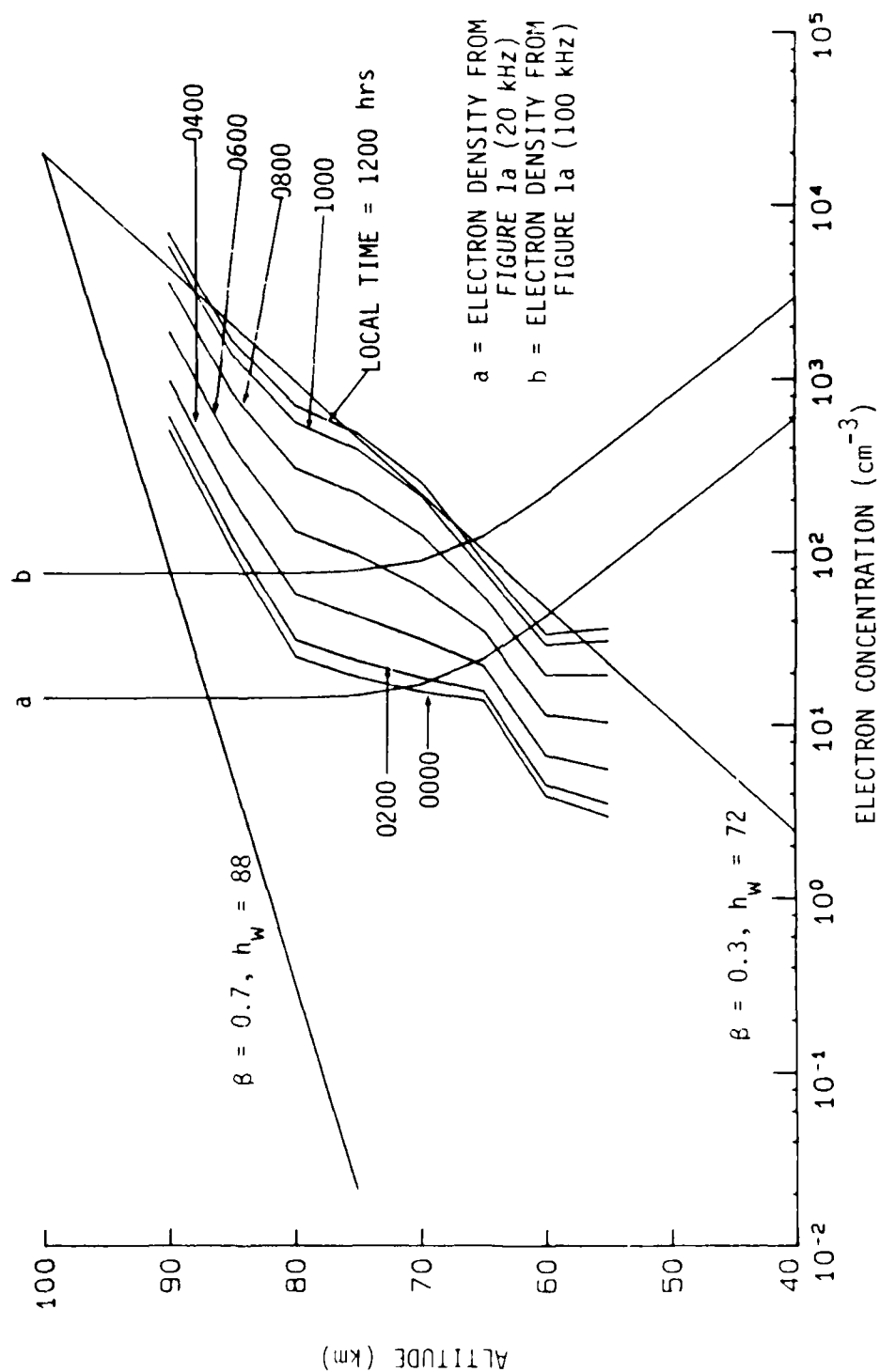


Figure 3. Electron concentration from McNamara's model (winter, magnetically quiet, low sunspot number, midlatitude conditions).

are also shown. It can be seen that the model agrees reasonably well with the daytime exponential, but produces electron concentrations significantly larger than the nighttime exponential.

## 2.3 PHYSICAL MODELS.

### 2.3.1 WECOM Models.

Physical models of D-region ionization for use in weapon effects prediction have been developed by Knapp (References 9 and 10) and Knapp and Jordano (Reference 11) and these models are regularly updated. The models incorporate results of very complex simulations of D-region chemistry and also tune results to match observed nuclear produced effects. Unfortunately the useful nuclear data are absorption data, are pertinent to medium to strong disturbance conditions, and provide little help in defining models for weak VLF/LF disturbance or recovery predictions. The models include a complex mixture of atomic and molecular species and associated reactions. In the model reactions between different species are combined for specific conditions to produce effective lumped-parameter reaction rate coefficients. The lumped-parameter coefficients are:

$$A = \text{attachment rate } s^{-1}$$

$$D = \text{detachment rate } s^{-1}$$

$$\alpha_i = \text{ion-ion recombination coefficient } cm^3 s^{-1}$$

$$\alpha_D = \text{ion-electron recombination coefficient } cm^3 s^{-1}.$$

These parameters are used in transient equations (Equations 11 through 14) and in quasi-equilibrium equations (Equations 15 through 17).

$$\frac{dN_e}{dt} = q - \alpha_D N_e N_+ - A N_e + D N_- \quad (11)$$

$$\frac{dN_-}{dt} = -\alpha_i N_- N_+ + A N_e - D N_- \quad (12)$$

$$\frac{dN_+}{dt} = q - \alpha_i N_- N_+ - \alpha_D N_e N_+ \quad (13)$$

$$N_+ = N_e + N_- \quad (14)$$

where

$q$  = ion production rate  $\text{cm}^{-3} \text{s}^{-1}$ .

$$N_+ = \sqrt{\frac{q}{\alpha}} \quad (15)$$

$$\alpha = \frac{A\alpha_i + D\alpha_D + \alpha_i\alpha_D \sqrt{\frac{q(A+D)}{A\alpha_i + D\alpha_D}}}{A + D + \alpha_i \sqrt{\frac{q(A+D)}{A\alpha_i + D\alpha_D}}} \quad (16)$$

$$N_e = \frac{q + D \sqrt{\frac{q}{\alpha}}}{A + D + \alpha_D \sqrt{\frac{q}{\alpha}}} \quad (17)$$

Equation 16 is solved iteratively for  $\alpha$ .

For normal ionosphere models, we will usually be interested in quasi-equilibrium solutions, although the limitation imposed by the transient equations on the decay from daytime profiles to desired nighttime profiles will be discussed.

Knapp (Reference 9) improved the VLF/LF predictions of the WEDCOM code (Reference 2) by incorporating the Berry model into the physical model. This was done by forcing the physical model to reproduce Berry's results over the altitude range

$$h_r \pm \frac{1}{\beta} \quad .$$

The force-fitting is done by adjusting the normal ion production rates to produce Berry's results. Berry's model results and the WEDCOM chemistry model results are sufficiently close together for most cases that this adjustment can be made while retaining reasonable values of ion production rates. In the WEDCOM code, only noon and midnight profiles are used.

More recently, the D-region model has been combined with a time-varying E- and F-region model used for HF. Knapp (Reference 9) has adjusted the model to merge smoothly into the empirical E-region model ionosphere. This is also done by adjusting normal production rates to include an effective  $q$  to match E-region electron densities above 90 km.

Figures 4 and 5 show electron concentration produced by the WECOM model as a function of altitude and parametric in time (two-hour periods) for mid-latitude summer and winter conditions. Tables 8 and 9 show the corresponding reaction rates for midnight and noon conditions. The exponential region (straight-line portion of the figures) that results from forcing Berry's results can be seen in the figures and, for the most part the transition points are reasonable.

As was the case for Berry's results, the nighttime electron concentrations are significantly higher in the 75 to 85 km altitude range than the hypothetical profile values used to match propagation data. Figures 6 and 7 show only the midnight and noon profiles from the WECOM model. Also shown on the figures are selected reference exponential profiles that have been found to reproduce some VLF and LF propagation data. A replot of Figure 1a, to emphasize the important reflecting region of the profiles is also shown on the figures. Note that the daytime profile and the proposed exponential profile are nearly equal in the reflecting range. The nighttime WECOM profile will produce reflection at significantly lower altitudes than the exponential profile and the irregularity at 75 and 85 km will have some effect on propagation predictions. Some possible adjustments to the physical model to produce a closer match to the nighttime exponentials are discussed in Section 3.

### 2.3.2 SIMBAL Models.

The SIMBAL code (Reference 1) includes a D-region model that was developed using an earlier (1981) version of D-region models used in weapon effects codes (then called WEPH VI, References 12 and 13). The procedure used was to compute  $N_e(h)$  and  $N_+(h)$  as a function of ion production  $Q(h)$ , with  $Q(h)$  varying from normal to about  $10^{10} \times$  normal. The electron and ion profiles were fit with equations of the form

$$N_e = \exp \{C_e + x \ln Q\} \quad (18)$$

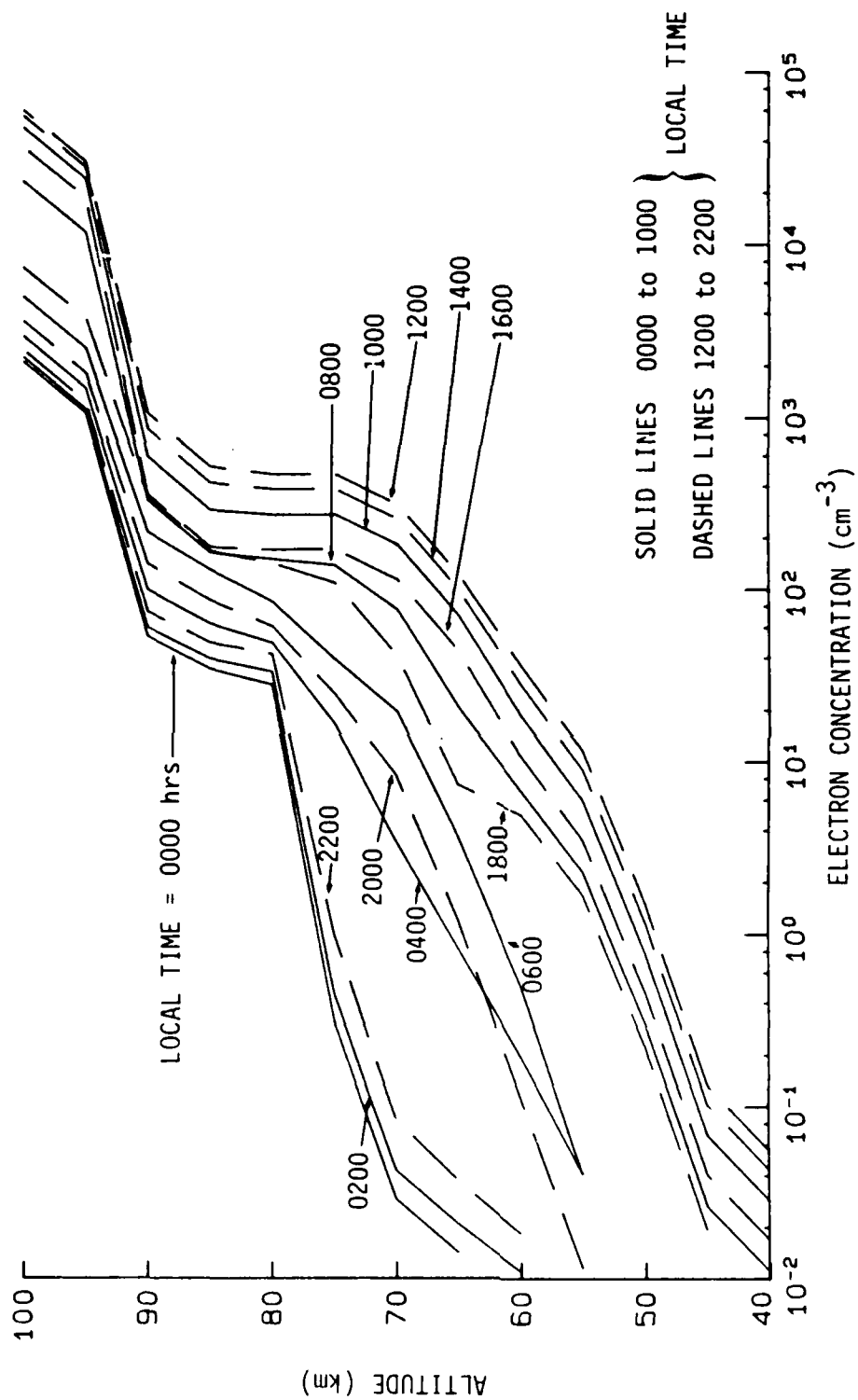


Figure 4. WECOM model electron concentration profiles for winter, 40 degrees latitude, SSN = 80.

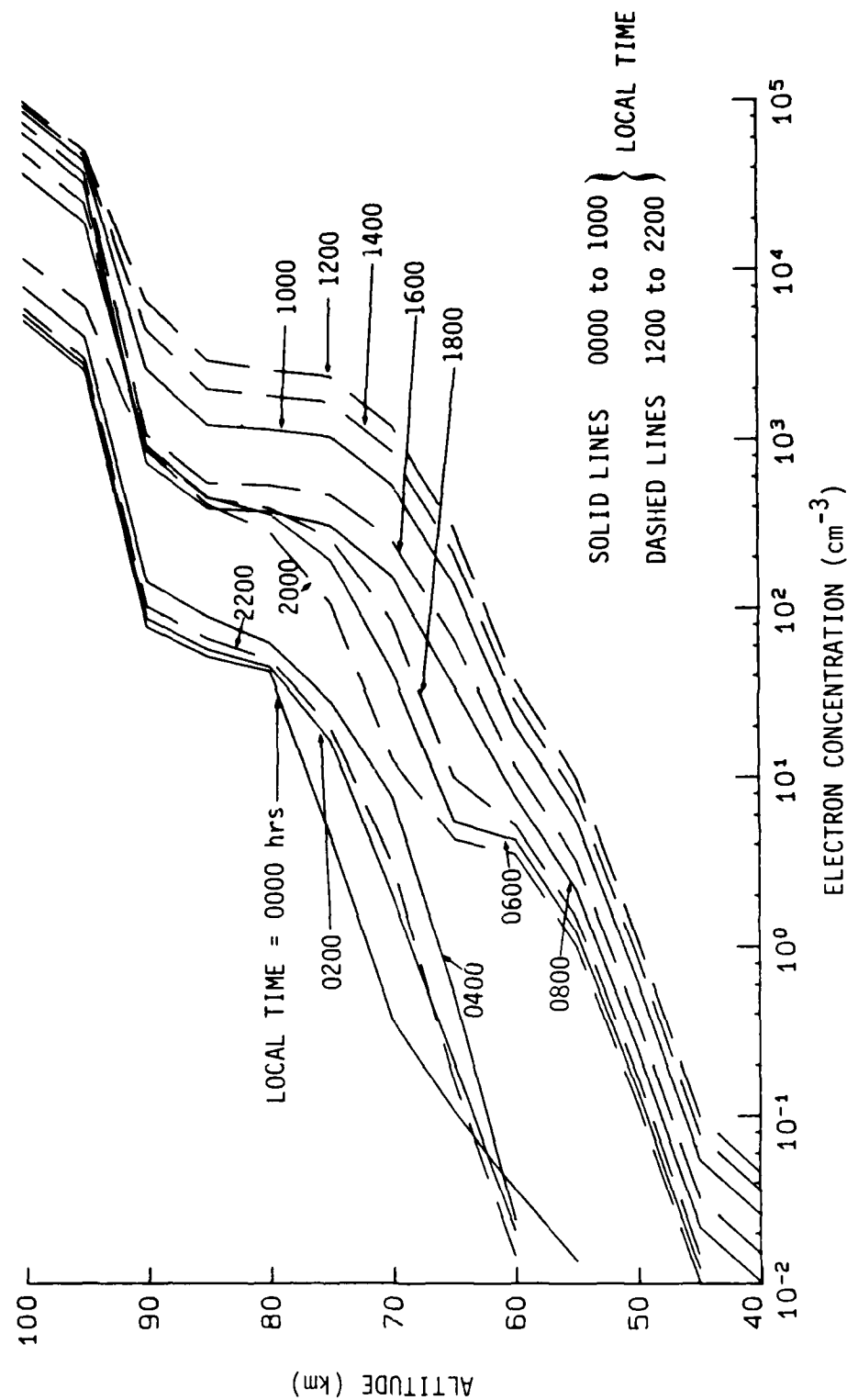


Figure 5. WECOM model electron concentration profiles for summer, 40 degrees latitude, SSN = 100.

Table 8. WECOM reaction rates for midlatitude winter conditions.

Height (km)	MIDNIGHT				
	$\alpha_i$	$\alpha_D$	D	A	$Q_a$
0.	3.20E-06	5.17E-06	9.67E-10	7.85E+07	2.86E-01
5.	2.36E-06	5.40E-06	5.29E-11	2.03E+07	2.91E+00
10.	1.75E-06	5.72E-06	5.56E-12	5.29E+06	8.17E+00
15.	1.02E-06	5.87E-06	1.98E-12	1.16E+06	9.25E+00
20.	5.06E-07	5.85E-06	2.17E-12	2.37E+05	6.09E+00
25.	2.56E-07	5.62E-06	3.86E-12	4.83E+04	3.06E+00
30.	1.49E-07	5.06E-06	7.35E-12	1.02E+04	1.32E+00
35.	9.99E-08	4.25E-06	2.72E-11	2.22E+03	6.18E-01
40.	7.90E-08	3.95E-06	1.24E-10	5.19E+02	2.93E-01
45.	6.99E-08	3.62E-06	4.72E-10	1.31E+02	1.44E-01
50.	6.62E-08	3.22E-06	1.01E-09	3.62E+01	7.50E-02
55.	6.58E-08	3.16E-06	8.04E-10	1.04E+01	4.09E-02
60.	6.64E-08	3.26E-06	3.00E-10	2.97E+00	2.22E-02
65.	6.77E-08	3.49E-06	7.33E-11	8.35E-01	1.19E-02
70.	6.93E-08	3.72E-06	1.26E-10	2.14E-01	6.27E-03
75.	7.12E-08	3.80E-06	5.76E-05	4.72E-02	3.23E-03
80.	7.32E-08	2.32E-06	1.93E-02	9.49E-03	2.78E-03
85.	7.45E-08	2.24E-06	2.39E-02	3.93E-03	3.15E-03
90.	7.42E-08	1.66E-06	2.16E-02	1.33E-03	4.94E-03
95.	7.24E-08	5.87E-07	4.15E-01	7.40E-04	6.57E-01
100.	7.04E-08	5.31E-07	1.60E+00	7.97E-04	2.35E+00

Height (km)	NOONTIME				
	$\alpha_i$	$\alpha_D$	D	A	$Q_a$
0.	3.20E-06	5.17E-06	2.98E-02	7.85E+07	1.39E-01
5.	2.36E-06	5.40E-06	2.94E-02	2.03E+07	1.41E+00
10.	1.75E-06	5.72E-06	2.73E-02	5.29E+06	3.97E+00
15.	1.02E-06	5.87E-06	2.70E-02	1.16E+06	4.49E+00
20.	5.06E-07	5.85E-06	2.77E-02	2.37E+05	2.96E+00
25.	2.56E-07	5.62E-06	2.82E-02	4.83E+04	1.49E+00
30.	1.49E-07	5.06E-06	2.83E-02	1.02E+04	6.41E-01
35.	9.99E-08	4.25E-06	2.68E-02	2.22E+03	3.00E-01
40.	7.90E-08	3.95E-06	2.14E-02	5.19E+02	1.42E-01
45.	6.99E-08	3.62E-06	1.73E-02	1.31E+02	7.00E-02
50.	6.62E-08	3.23E-06	7.75E-02	3.61E+01	3.63E-02
55.	6.58E-08	3.09E-06	3.66E-01	1.04E+01	1.97E-02
60.	6.64E-08	3.01E-06	1.63E+00	2.92E+00	1.14E-02
65.	6.77E-08	3.02E-06	3.84E+00	7.78E-01	5.34E-02
70.	6.93E-08	2.74E-06	5.30E+00	1.93E-01	2.78E-01
75.	7.12E-08	2.15E-06	7.74E+00	4.42E-02	4.75E-01
80.	7.32E-08	2.02E-06	1.23E+01	9.49E-03	4.42E-01
85.	7.45E-08	1.65E-06	2.06E+01	2.35E-03	4.42E-01
90.	7.42E-08	7.97E-07	3.56E+01	6.80E-04	8.79E-01
95.	7.24E-08	4.70E-07	8.39E+01	6.20E-04	4.32E+02
100.	7.04E-08	4.41E-07	1.17E+02	7.83E-04	1.56E+03

Table 9. WECOM reaction rates for midlatitude summer conditions.

Height (km)	<u>MIDNIGHT</u>				
	$\alpha_i$	$\alpha_D$	D	A	$Q_a$
0.	2.58E-06	5.00E-06	3.29E-08	8.81E+07	7.24E-01
5.	2.06E-06	5.27E-06	4.70E-10	2.12E+07	5.99E+00
10.	1.66E-06	5.62E-06	1.88E-11	5.89E+06	1.74E+01
15.	1.09E-06	5.88E-06	2.94E-12	1.36E+06	2.17E+01
20.	5.18E-07	5.77E-06	4.77E-12	2.76E+05	1.46E+01
25.	2.54E-07	5.26E-06	1.24E-11	5.77E+04	7.57E+00
30.	1.45E-07	4.45E-06	3.38E-11	1.27E+04	3.39E+00
35.	9.86E-08	4.04E-06	1.22E-10	2.95E+03	1.69E+00
40.	7.87E-08	3.82E-06	4.48E-10	7.33E+02	8.90E-01
45.	6.96E-08	3.45E-06	1.49E-09	1.95E+02	5.05E-01
50.	6.59E-08	3.03E-06	3.24E-09	5.54E+01	3.19E-01
55.	6.54E-08	2.96E-06	2.80E-09	1.65E+01	2.26E-01
60.	6.61E-08	3.09E-06	1.17E-09	4.82E+00	1.74E-01
65.	6.80E-08	3.55E-06	3.45E-10	1.38E+00	1.45E-01
70.	7.08E-08	4.09E-06	1.03E-09	3.48E-01	1.28E-01
75.	7.41E-08	4.32E-06	1.89E-04	7.21E-02	1.19E-01
80.	7.81E-08	3.34E-06	3.59E-02	1.25E-02	8.12E-03
85.	8.15E-08	2.75E-06	3.45E-02	3.65E-03	8.14E-03
90.	7.93E-08	2.39E-06	2.70E-02	1.07E-03	1.52E-02
95.	7.72E-08	6.45E-07	8.57E-01	5.95E-04	4.26E+00
100.	7.48E-08	5.66E-07	3.04E+00	6.01E-04	1.47E+01

Height (km)	<u>NOONTIME</u>				
	$\alpha_i$	$\alpha_D$	D	A	$Q_a$
0.	2.58E-06	5.00E-06	2.98E-02	8.81E+07	1.45E-01
5.	2.06E-06	5.27E-06	2.94E-02	2.12E+07	1.38E+00
10.	1.66E-06	5.62E-06	2.73E-02	5.89E+06	4.08E+00
15.	1.09E-06	5.88E-06	2.70E-02	1.36E+06	5.08E+00
20.	5.18E-07	5.77E-06	2.77E-02	2.76E+05	3.42E+00
25.	2.54E-07	5.26E-06	2.82E-02	5.77E+04	1.75E+00
30.	1.45E-07	4.45E-06	2.83E-02	1.27E+04	7.71E-01
35.	9.86E-08	4.04E-06	2.69E-02	2.95E+03	3.72E-01
40.	7.87E-08	3.82E-06	2.19E-02	7.33E+02	1.83E-01
45.	6.96E-08	3.45E-06	1.64E-02	1.95E+02	9.30E-02
50.	6.59E-08	3.08E-06	7.22E-02	5.53E+01	4.92E-02
55.	6.54E-08	2.94E-06	3.53E-01	1.65E+01	2.72E-02
60.	6.61E-08	2.91E-06	1.67E+00	4.77E+00	1.64E-02
65.	6.80E-08	3.16E-06	4.19E+00	1.31E+00	3.70E-01
70.	7.08E-08	3.12E-06	6.23E+00	3.22E-01	4.75E+00
75.	7.41E-08	2.25E-06	9.69E+00	6.87E-02	1.26E+01
80.	7.81E-08	2.12E-06	1.53E+01	1.25E-02	1.43E+01
85.	8.15E-08	1.78E-06	2.34E+01	2.29E-03	1.53E+01
90.	7.93E-08	6.83E-07	3.44E+01	5.63E-04	3.01E+01
95.	7.72E-08	4.45E-07	7.14E+01	5.11E-04	1.15E+03
100.	7.48E-08	4.13E-07	8.87E+01	5.93E-04	4.06E+03



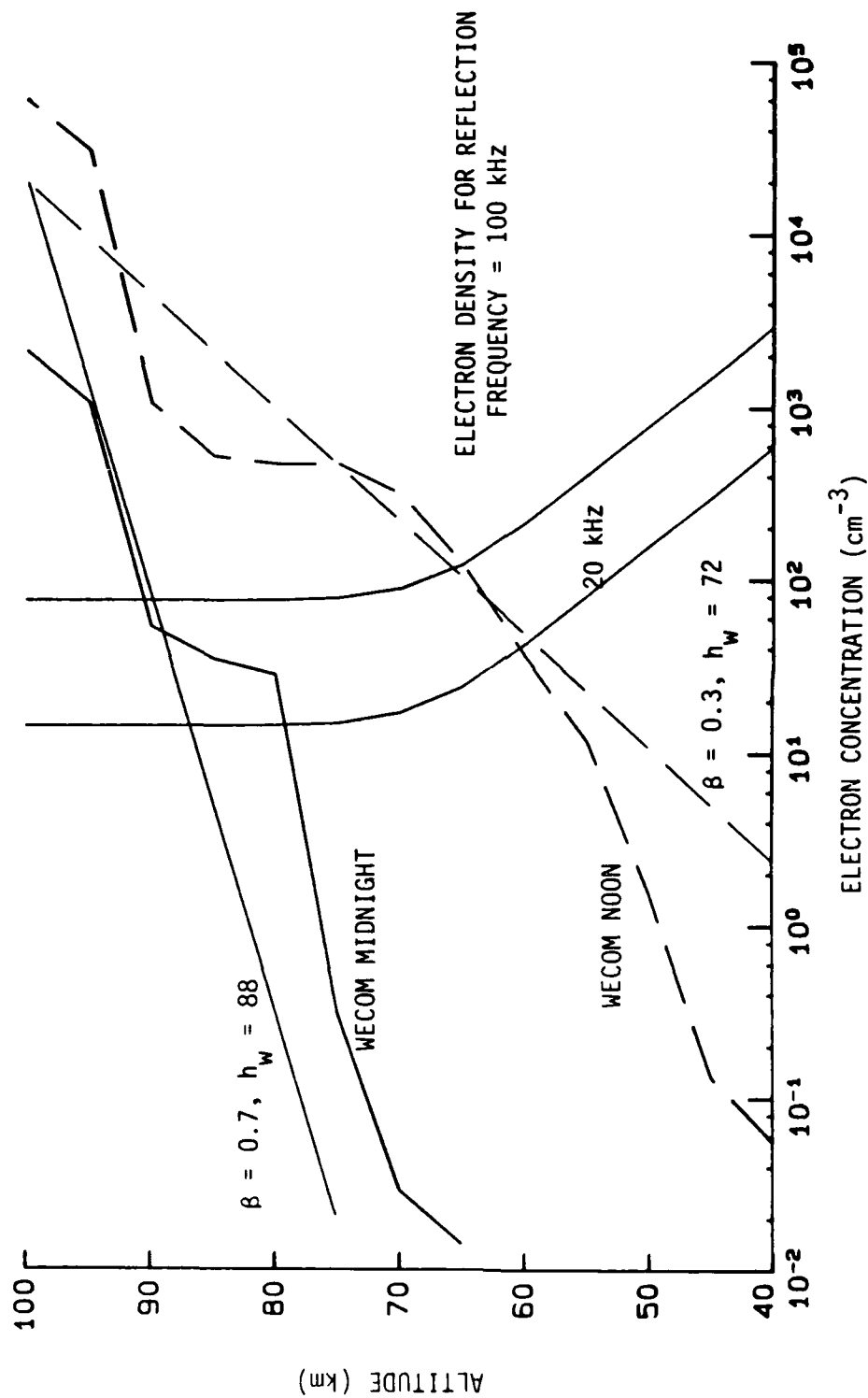


Figure 6. WECOM noon and midnight profiles compared to widely used exponential profiles for winter, 40 degrees latitude, SSN = 80.

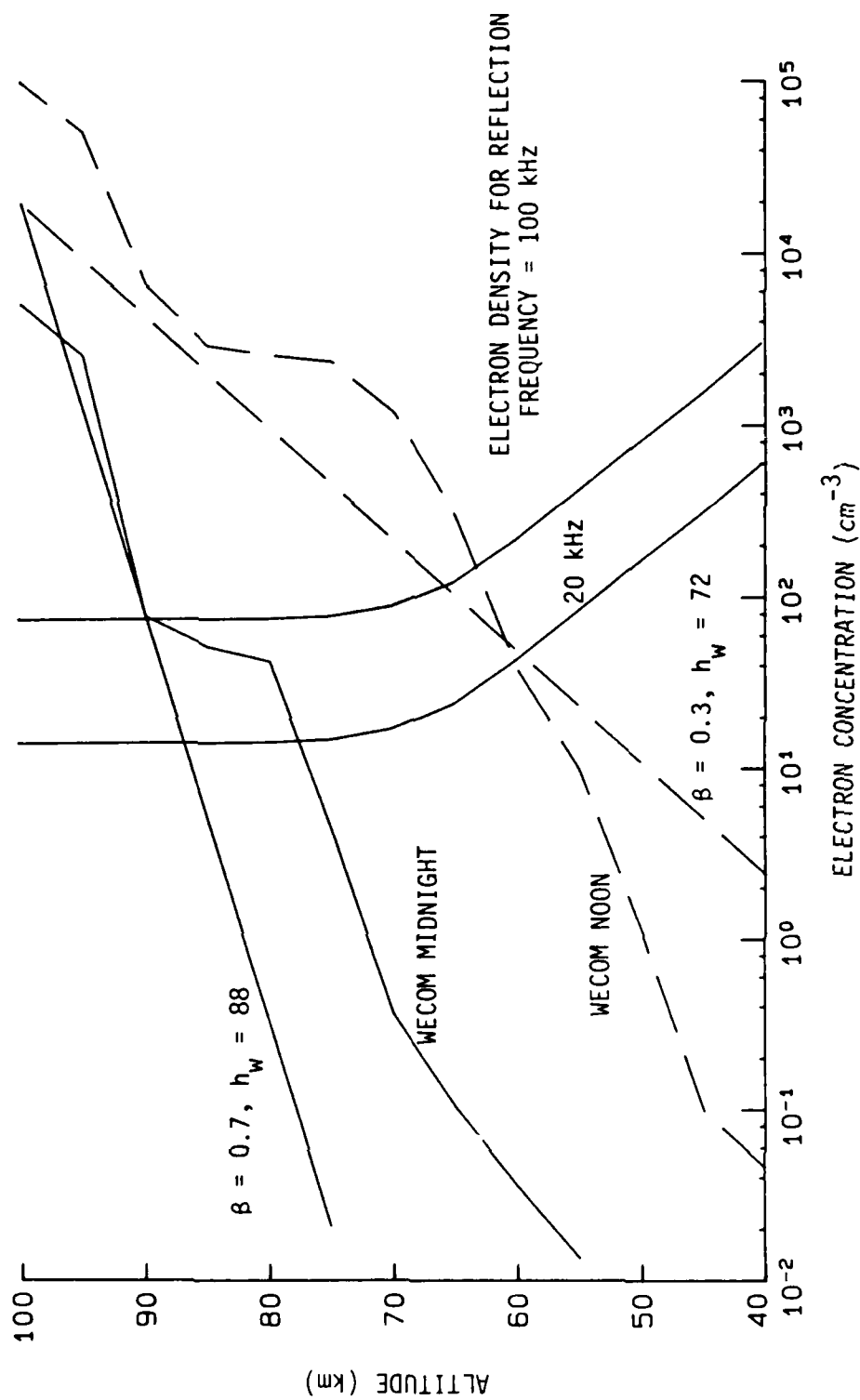


Figure 7. WECOM noon and midnight profiles compared to widely used exponential profiles for summer, 40 degrees latitude, SSN = 100.

$$N_+ = \exp (C_+ + y \ln Q) \quad (19)$$

where there are one or two sets of  $C_e$ 's,  $C_+$ 's,  $x$ 's, and  $y$ 's for each altitude. Two sets are required - one set for large  $Q$ , one set for small  $Q$  at some altitudes. Equations 18 and 19 are more efficient than the quasi-equilibrium equations. They also have the advantage of including the dependence of the lumped-parameter reaction rates on production rate.

Figure 8 shows SIMBAL normal electron density concentration compared to selected exponential profiles. In the SIMBAL program only day (noon) and night (midnight) profiles are used. Transition across the day-night terminator is abrupt. Comparison of Figure 8 with Figures 6 and 7 shows that the SIMBAL daytime model is relatively consistent with the newer WECOM model and the SIMBAL normal nighttime model is intermediate between the summer and winter nighttime values for WECOM.

The nighttime VLF loss rates estimated using the SIMBAL nighttime profiles are higher than most observed values and this discrepancy has resulted in requests by SIMBAL code users to define a revised model that would produce predictions which agree better with observed losses. Some comparisons between SIMBAL and measured data are shown in Figures 9 through 12. The SIMBAL program, which is normally used to compute propagation effects between two fixed locations, uses a RMS mode or hop sum instead of a vector sum, to avoid sensitivity to predicting the location of peaks and nulls. The RMS sum results in a smooth variation in field strength versus distance. The SIMBAL field strengths have, in general, the correct magnitude for daytime conditions, but are generally lower than measured values for nighttime conditions.

Results are also shown from the VLFSIM program (Reference 14), which uses the RMS summing technique similar to SIMBAL, but the undisturbed ionosphere model has been modified to use precomputed mode constants for the  $\beta = 0.7$ ,  $h_w = 88$  km profile. Predictions using VLFSIM show generally better agreement with measured data for nighttime conditions than the SIMBAL results.

The technique used to force the VLFSIM ionosphere model to relax to the exponential profile for no disturbance is discussed in Section 3.

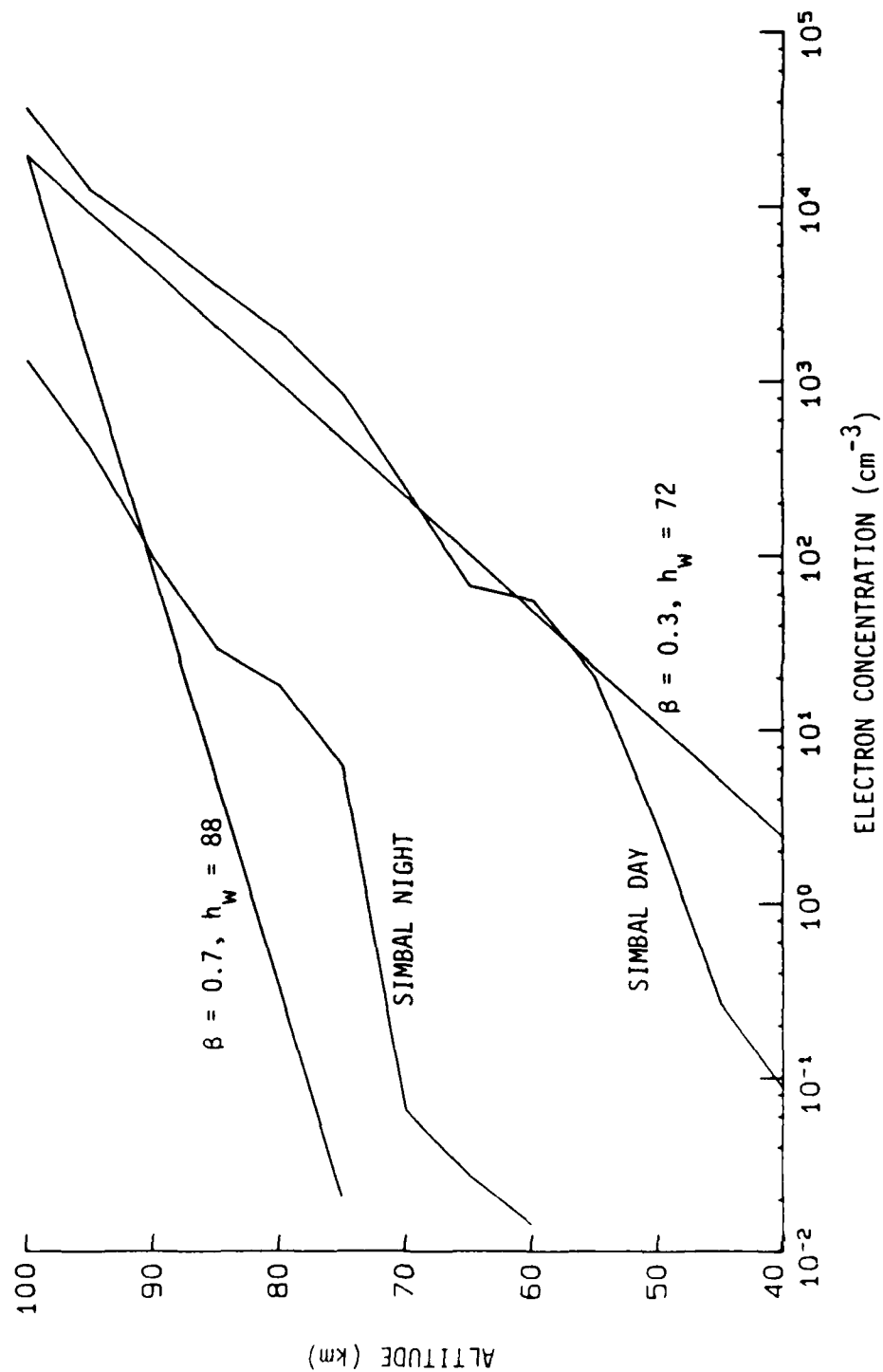


Figure 8. SIMBAL day and night profiles compared to widely used exponential profiles.

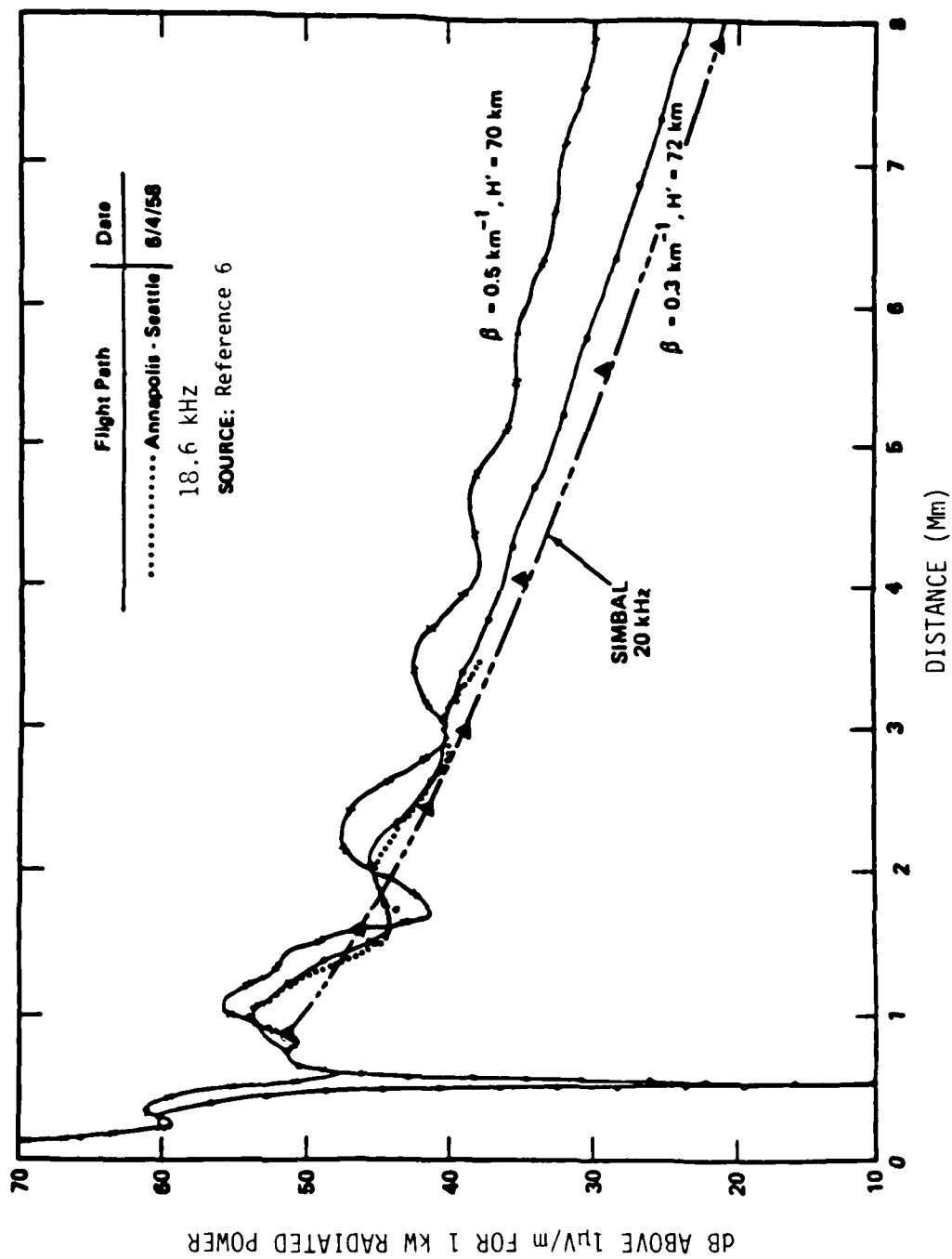


Figure 9. Comparison of SIMBAL 20 kHz daytime predictions with data and calculations from Reference 6.

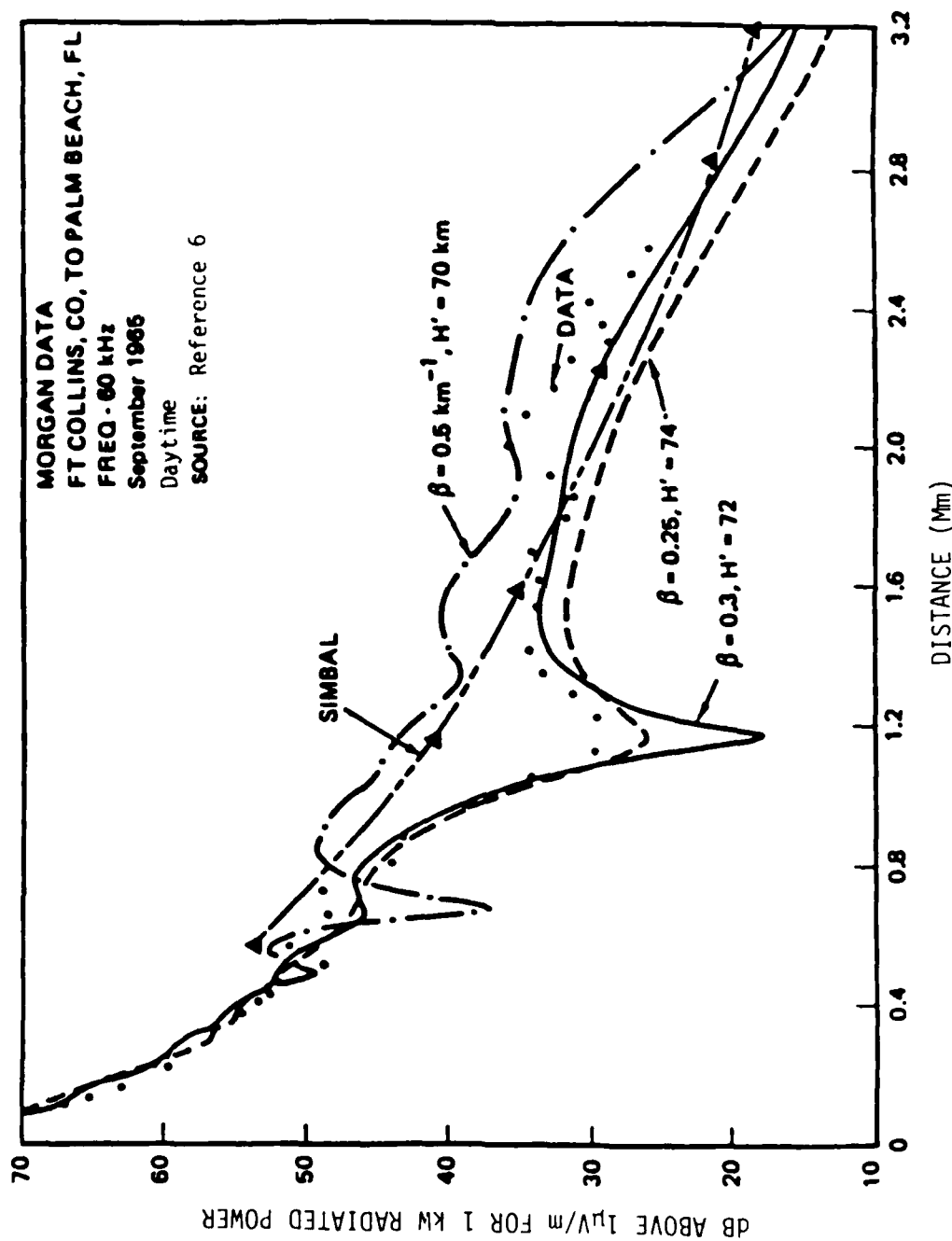


Figure 10. Comparison of SIMBAL 60 kHz daytime predictions with data and calculations from Reference 6.

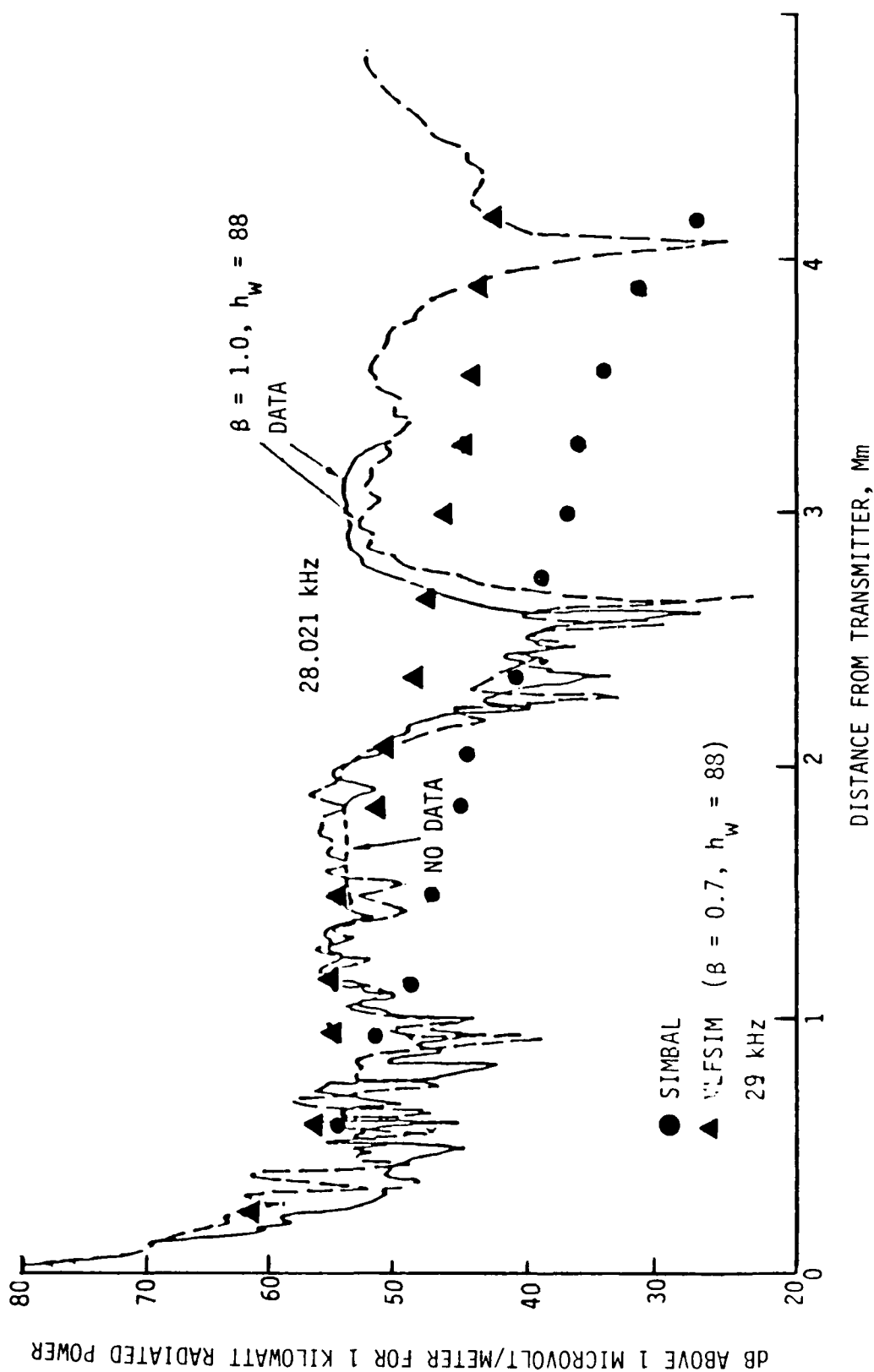


Figure 11. Comparison of SIMBAL and VLFSIM 29 kHz nighttime predictions with data and calculations from Reference 6.

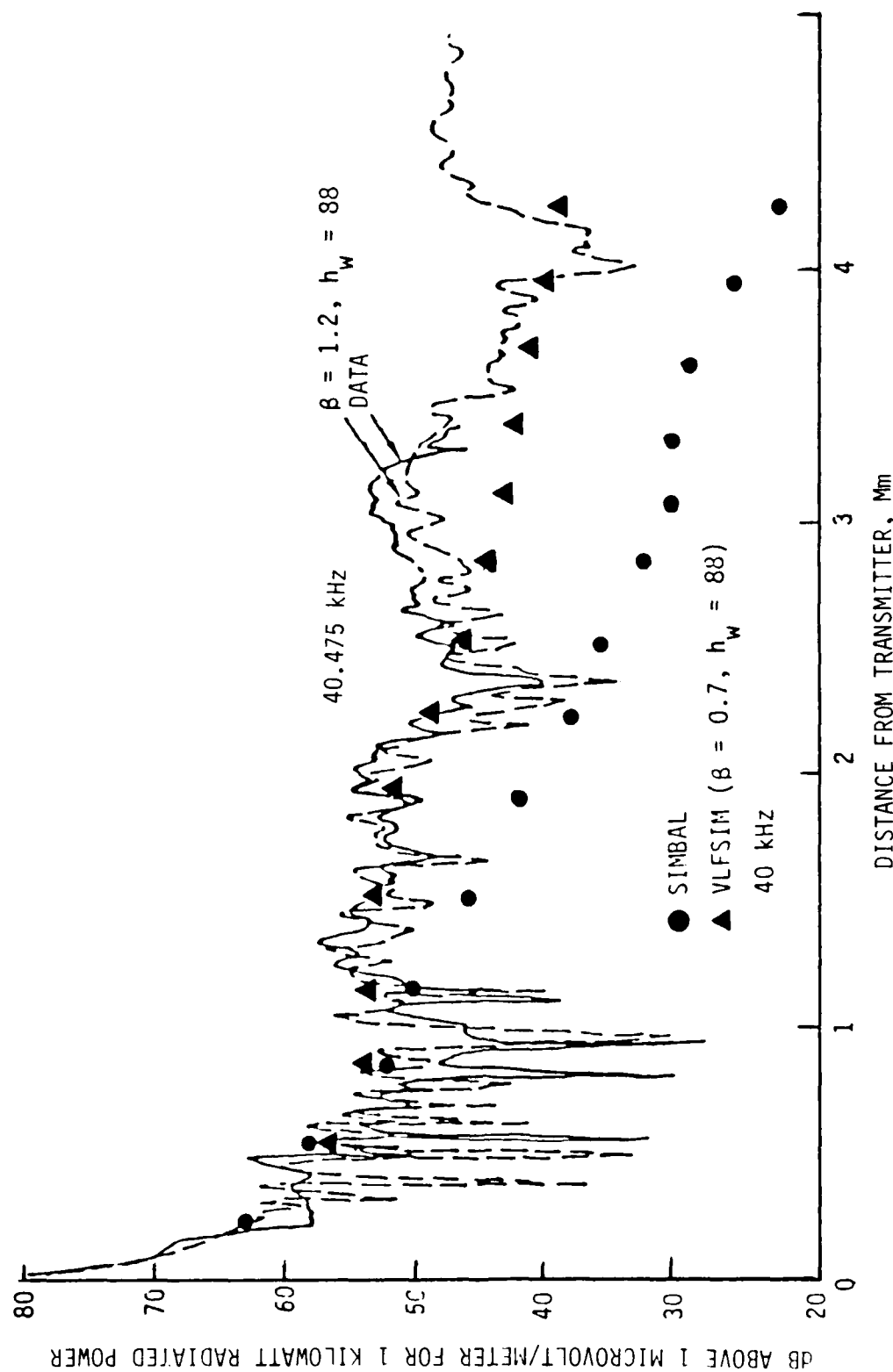


Figure 12. Comparison of SIMBAL and VLFSIM 40 kHz nighttime predictions with data and calculations from Reference 6.



#### 2.4 PROFILES TO MATCH HF ABSORPTION PREDICTIONS.

HF D-region absorption is predicted by integrating the absorption through the D and lower E region or by using empirical models that estimate absorption directly. The most recent CCIR approved model is used in IONCAP (Reference 15) and computes the absorption per semi-hop using

$$A \text{ (dB)} = \frac{338 I \sec \phi}{(f + f_H)^{1.98} + 10.2} \quad (20)$$

where

- $f$  = wave frequency (MHz)
- $f_H$  = longitudinal component of the gyrofrequency (MHz)
- $\phi$  = angle of incidence of the ray at the D region.

$$I = -0.04 + \exp (-2.937 + 0.8445 f_{oE}) \quad (21)$$

where

$f_{oE}$  = E-layer critical frequency.

The WECOM model is compared to the empirical predictions by integrating vertical one-way absorption through the D-region profiles shown in Figures 4 and 5 and comparing to results produced using Equations 20 and 21. The profiles and the E-layer critical frequency were both computed using an analytic model (Reference 16) for the E-region parameters. The values obtained for a frequency of 10 MHz are shown in Table 10.

The integral and empirical values agree reasonably well near summer noon, but are about a factor of 2 low for other times (when absorption is important). An increase in electron density above about 70 km for daytime conditions would improve the agreement between the two models and have little affect on VLF/LF propagation predictions.

HF absorption data and associated models provide no useful information to deduce nighttime profiles for VLF/LF propagation.

Table 10. One-way vertical absorption at 10 MHz,  
latitude = 40 degrees, SSN = 100.

Local Time (hr)	Summer			Winter		
	FOE (MHz)	Empirical (dB)	Integral (dB)	FOE (MHz)	Empirical (dB)	Integral (dB)
0	0.787	0.17	$3.48^{-2}$	0.52	0.12	$2.31^{-2}$
2	0.816	0.18	$4.57^{-2}$	0.54	0.12	$2.50^{-2}$
4	0.989	0.23	$6.39^{-2}$	0.62	0.13	$4.10^{-2}$
6	2.21	0.83	0.38	0.81	0.18	$6.57^{-2}$
8	3.00	1.72	0.58	1.80	0.55	0.32
10	3.54	2.79	1.46	2.67	1.28	0.70
12	3.78	3.44	2.68	3.01	1.74	1.03
14	3.68	3.15	2.04	2.89	1.56	0.90
16	3.26	2.17	0.883	2.31	0.91	0.50
18	2.58	1.17	0.497	0.99	0.22	0.15
20	1.20	0.29	0.147	0.69	0.15	$4.10^{-2}$
22	0.865	0.19	$4.62^{-2}$	0.57	0.12	$2.00^{-2}$

### SECTION 3

#### ADJUSTING PROFILES TO MATCH PROPAGATION DATA

##### 3.1 GENERAL.

The previous sections have provided some comparisons between D-region electron concentration profiles produced by selected D-region ionosphere models and profiles inferred from comparisons between measured and predicted VLF and LF propagation data. The differences between model profiles and profiles required to match data are not great for daytime conditions, but are frequently large for nighttime conditions. In general, the propagation predictions require a lower electron concentration in the altitude range from 75 to 95 km than the models produce.

A coordinated program to simultaneously collect electron concentration measurements and propagation measurements over a period of time would be required to completely resolve model differences. However, VLF and LF propagation parameters do provide a sensitive measure of low-concentration profile properties, and there is good reason to have model predictions reproduce measured data in the undisturbed case as a starting or recovery point for nuclear disturbed predictions.

Two model parameters (ion production rate and atmospheric chemistry reaction rates) can be adjusted separately or jointly to force model profiles to take on prescribed values. The method chosen to make the adjustment should use values that are within the bounds of uncertainty of the parameters. Also, as will be shown later, the effects of adjusting the two sets of parameters are sometimes coupled and must be considered jointly.

Reducing the normal ion production rate to reduce electron density to match selected profiles will result in increasing the sensitivity to low levels of weapon ionization. On the other hand, modifying the chemistry to decrease electron density will decrease the sensitivity to low level disturbances.

In the following subsections, the altitude region where profile matching is required, and procedures for matching specified profiles are addressed.

### 3.2 ALTITUDE REGIONS FOR MATCHING.

Equations 2 and 3 can be used to define altitudes where VLF reflection maximizes. Detailed calculations of ionospheric reflection coefficients from two selected exponential profiles were performed to estimate the altitude range over which a smooth exponential variation must be maintained to provide answers nearly the same as obtained when the exponential profile is assumed for all altitudes. The profiles examined were selected to be ( $\beta = 0.3$ ,  $h_w = 72$ ) for daytime and ( $\beta = 0.7$ ,  $h_w = 88$ ) for nighttime. The calculations tested to define upper and lower altitudes where a change of slope could be introduced without changing the reflection coefficient values.

The actual profiles used in the analysis were:

$$N_e(h) = N_o \exp(-0.7 \times 88) \exp(0.55 h), \quad h_\ell < h < h_u$$

$$N_e(h) = N_e(h_\ell) \exp(0.35 (h - h_\ell)) \quad h < h_\ell$$

$$N_e(h) = N_e(h_u) \exp(0.35 (h - h_u)) \quad h > h_u$$

for nighttime and

$$N_e(h) = N_o \exp(-0.3 \times 72) \exp(0.15 h), \quad h_\ell < h < h_u$$

$$N_e(h) = N_e(h_\ell) \exp(0.3 (h - h_\ell)) \quad h < h_\ell$$

$$N_e(h) = N_e(h_u) \exp(0.3 (h - h_u)) \quad h > h_u$$

for daytime conditions where

$$N_o = 1.43 \times 10^7 \text{ electrons/cm}^3.$$

The changes in slope approximate changes required to cause the exponential profile to join smoothly with other model profiles. Calculations were performed to show sensitivity to values chosen for  $h_\ell$  and  $h_u$ .

Table 11 shows the results for the nighttime calculations. The results show the four components of the anisotropic reflection coefficient calculation for a frequency of 30 kHz and 3 different real incident angles. The reflection coefficient amplitude components are:

Table 11. Reflection coefficients as a function of break points in the exponential profile,  $\beta = 0.7$ ,  $h_w = 88$ , frequency = 30 kHz.

Upper Break Altitude (km)	Lower Break Altitude (km)	Angle of Incidence (deg)	<u>R11</u>			<u>R22</u>			<u>R21</u>			<u>R12</u>		
100	60	78	5.87E-01	3.51E-02	1.91E-01	-8.27E-01	8.72E-02	3.12E-01	9.32E-02	2.38E-01				
		80	5.46E-01	3.56E-01	7.26E-01	-4.85E-01	-1.03E-01	2.66E-01	6.15E-02	2.22E-01				
		82	3.29E-01	6.38E-01	8.87E-01	1.46E-01	-2.04E-01	1.28E-01	-1.56E-01	1.21E-01				
95	60	78	5.87E-01	3.52E-02	1.90E-01	-8.27E-01	8.73E-02	3.12E-01	9.35E-02	2.38E-01				
		80	5.46E-01	3.56E-01	7.25E-01	-4.86E-01	-1.03E-01	2.66E-01	-6.13E-02	2.22E-01				
		82	3.28E-01	6.36E-01	8.87E-01	1.45E-01	-2.04E-01	1.28E-01	-1.56E-01	1.21E-01				
94	60	78	5.87E-01	3.58E-02	1.84E-01	-8.27E-01	8.81E-02	3.12E-01	9.61E-02	2.40E-01				
		80	5.46E-01	3.57E-01	7.21E-01	-4.89E-01	-1.03E-01	2.67E-01	-6.07E-02	2.25E-01				
		82	3.28E-01	6.39E-01	8.86E-01	1.41E-01	-2.04E-01	1.29E-01	-1.57E-01	1.24E-01				
93	60	78	5.85E-01	3.59E-02	1.63E-01	-8.29E-01	9.36E-02	3.12E-01	1.00E-01	2.44E-01				
		80	5.45E-01	3.56E-01	7.10E-01	-5.02E-01	-9.99E-02	2.69E-01	-6.00E-02	2.29E-01				
		82	3.28E-01	6.38E-01	8.87E-01	1.28E-01	-2.04E-01	1.32E-01	-1.59E-01	1.27E-01				
92	60	78	5.80E-01	3.39E-02	1.08E-01	-8.34E-01	1.10E-01	3.11E-01	1.11E-01	2.48E-01				
		80	5.43E-01	3.52E-01	6.80E-01	-5.36E-01	-9.06E-02	2.77E-01	-5.62E-02	2.38E-01				
		82	3.29E-01	6.35E-01	8.88E-01	9.17E-02	-2.03E-01	1.40E-01	-1.62E-01	1.34E-01				
91	60	78	5.74E-01	3.19E-02	-1.19E-02	-8.34E-01	1.41E-01	3.06E-01	1.37E-01	2.53E-01				
		80	5.41E-01	3.47E-01	6.10E-01	-6.05E-01	-7.13E-02	2.91E-01	-4.42E-02	2.57E-01				
		82	3.30E-01	6.31E-01	8.86E-01	1.48E-02	-2.00E-01	1.57E-01	-1.66E-01	1.52E-01				
90	60	78	5.64E-01	3.54E-02	-2.16E-01	-7.97E-01	1.90E-01	2.85E-01	1.84E-01	2.53E-01				
		80	5.35E-01	3.44E-01	4.76E-01	-7.05E-01	-3.59E-02	3.05E-01	-1.84E-02	2.85E-01				
		82	3.30E-01	6.26E-01	8.70E-01	-1.15E-01	-1.91E-01	1.81E-01	-1.69E-01	1.82E-01				
100	70	78	5.87E-01	3.51E-02	1.91E-01	-8.27E-01	8.72E-02	3.12E-01	9.32E-02	2.38E-01				
		80	5.46E-01	3.56E-01	7.26E-01	-4.85E-01	-1.03E-01	2.66E-01	-6.15E-02	2.22E-01				
		82	3.29E-01	6.38E-01	8.87E-01	1.46E-01	-2.04E-01	1.28E-01	-1.56E-01	1.21E-01				

Table 11. Reflection coefficients as a function of break points in the exponential profile,  $\beta = 0.7$ ,  $h_w = 88$ , frequency = 30 kHz (Concluded).

Upper Break Altitude (km)	Lower Break Altitude (km)	Angle of Incidence (deg)	<u>R11</u>			<u>R22</u>			<u>R21</u>			<u>R12</u>		
100	75	78	5.87E-01	3.51E-02	1.91E-01	-8.27E-01	8.72E-02	3.12E-01	9.32E-02	2.38E-01				
		80	5.46E-01	3.56E-01	7.26E-01	-4.85E-01	-1.03E-01	2.66E-01	-6.15E-02	2.22E-01				
		82	3.29E-01	6.38E-01	8.87E-01	1.46E-01	-2.04E-01	1.28E-01	-1.56E-01	1.21E-01				
100	76	78	5.86E-01	-4.16E-02	8.18E-02	-8.45E-01	1.27E-01	2.98E-01	1.23E-01	2.24E-01				
		80	5.81E-01	2.94E-01	6.68E-01	-5.61E-01	-7.36E-02	2.75E-01	-3.72E-02	2.27E-01				
		82	3.83E-01	6.07E-01	8.96E-01	6.75E-02	-1.92E-01	1.45E-01	-1.45E-01	1.34E-01				
100	77	78	5.54E-01	-1.91E-01	-1.39E-01	-8.37E-01	1.99E-01	2.55E-01	1.77E-01	1.85E-01				
		80	6.29E-01	1.61E-01	5.31E-01	-6.93E-01	-1.25E-02	2.85E-01	1.23E-02	2.30E-01				
		82	4.81E-01	5.30E-01	8.94E-01	-8.94E-02	-1.64E-01	1.76E-01	-1.20E-01	1.57E-01				
100	78	78	4.83E-01	-3.26E-01	-3.51E-01	-7.72E-01	2.58E-01	1.95E-01	2.18E-01	1.33E-01				
		80	6.46E-01	2.16E-02	3.68E-01	-7.91E-01	4.89E-02	2.80E-01	6.07E-02	2.22E-01				
		82	5.63E-01	4.37E-01	8.64E-01	-2.44E-01	-1.31E-01	2.02E-01	-9.17E-02	1.75E-01				
100	79	78	3.80E-01	-4.36E-01	-5.39E-01	6.55E-01	2.98E-01	1.22E-01	2.44E-01	7.38E-02				
		80	6.30E-01	-1.17E-01	1.87E-01	-8.51E-01	1.07E-01	2.63E-01	1.06E-01	2.04E-01				
		82	6.24E-01	3.31E-01	8.07E-01	-3.90E-01	-9.42E-02	2.21E-01	-6.17E-02	1.88E-01				
100	80	78	2.51E-01	-5.10E-01	-6.90E-01	-4.93E-01	3.18E-01	4.20E-02	2.54E-01	1.10E-02				
		80	5.81E-01	-2.44E-01	-2.17E-03	-8.71E-01	1.60E-01	2.33E-01	1.45E-01	1.78E-01				
		82	6.61E-01	2.17E-01	7.25E-01	-5.24E-01	-5.55E-02	2.33E-01	-3.14E-02	1.96E-01				
95	70	78	5.87E-01	3.52E-02	1.90E-01	8.27E-01	8.73E-02	3.12E-01	9.35E-02	2.38E-01				
		80	5.46E-01	3.56E-01	7.25E-01	-4.86E-01	-1.03E-01	2.66E-01	-6.13E-02	2.22E-01				
		82	3.28E-01	6.38E-01	8.87E-01	1.45E-01	-2.04E-01	1.28E-01	-1.56E-01	1.21E-01				

- $R_{11}$  = vertical incidence - vertical reflection
- $R_{22}$  = horizontal incidence - horizontal reflection
- $R_{12}$  = vertical incidence - horizontal reflection
- $R_{21}$  = horizontal incidence - vertical reflection.

The nighttime reference condition, where it could be easily demonstrated that the changes in slope had no effect, were for an upper break point ( $h_u$ ) of 100 km and a lower break point ( $h_l$ ) of 60 km.

It can be seen from the table that raising the lower break point above 75 km or lowering the upper break point below 95 km causes the reflection coefficient to change from the reference condition.

Results from a similar analysis for daytime conditions are shown in Table 12. Here the reference condition is for an upper break point of 75 km and a lower break point of 40 km. The results show that the upper break point could be as low as 70 km and the lower break point as high as 45 km without changing the results.

Thus to reproduce calculations that are made with a fictitious exponential profile at all altitudes, the exponential range must extend over an altitude range of 20 to 30 km.

### 3.3 NUMERICAL FIT PROCEDURE.

The numerical fit used as an ionosphere model for the SIMBAL program (Section 2-3.2) provides a simple mechanism to adjust electron concentration profiles. The equation (see Equation 18) for electron concentration in undisturbed conditions is

$$N_e = \exp (C_e + x \ln Q)$$

where the values for  $C_e$  and  $x$  are determined from fits to data calculated with detailed chemistry models. In the altitude range of interest,  $x$  is near 0.5, as expected from the electron dependence on the square root of  $Q$ . Several procedures were tested by adjusting  $C_e$  and/or  $Q$  to obtain the exponential concentration where there is no disturbance and to transition smoothly into the model based on chemistry for a moderate disturbance. The

Table 12. Reflection coefficients as a function of break points in the exponential profile,  $\beta = 0.3$ ,  $h_w = 72$ , frequency = 30 kHz.

Upper Break Altitude (km)	Lower Break Altitude (km)	Angle of Incidence (deg)	<u>R11</u>			<u>R22</u>			<u>R21</u>			<u>R12</u>		
75	40	78	-1.89E-01	-1.85E-01	-1.54E-01	-1.17E-01	2.76E-02	1.06E-02	2.62E-02	2.62E-02	-3.08E-02	2.62E-02	-3.08E-02	
		80	6.49E-02	-3.22E-01	2.64E-02	-2.63E-01	4.55E-03	2.85E-02	3.82E-02	3.82E-02	5.82E-03	3.82E-02	5.82E-03	
		82	3.77E-01	-1.64E-01	3.13E-01	-1.66E-01	-2.03E-02	1.80E-02	1.51E-02	1.51E-02	3.22E-02	1.51E-02	3.22E-02	
74	40	78	-1.89E-01	-1.85E-01	-1.54E-01	-1.17E-01	2.76E-02	1.06E-02	2.62E-02	2.62E-02	-3.08E-02	2.62E-02	-3.08E-02	
		80	6.49E-02	-3.22E-01	2.64E-02	-2.63E-01	4.54E-03	2.85E-02	3.82E-02	3.82E-02	5.82E-03	3.82E-02	5.82E-03	
		82	3.77E-01	-1.64E-01	3.13E-01	-1.66E-01	-2.03E-02	1.80E-02	1.51E-02	1.51E-02	3.22E-02	1.51E-02	3.22E-02	
72	40	78	-1.89E-01	-1.85E-01	-1.55E-01	-1.18E-01	2.74E-02	1.06E-02	2.62E-02	2.62E-02	-3.05E-02	2.62E-02	-3.05E-02	
		80	6.47E-02	-3.22E-01	2.65E-02	-2.64E-01	4.46E-03	2.84E-02	3.80E-02	3.80E-02	5.92E-03	3.80E-02	5.92E-03	
		82	3.76E-01	-1.65E-01	3.13E-01	-1.66E-01	-2.02E-02	1.79E-02	1.49E-02	1.49E-02	3.22E-02	1.49E-02	3.22E-02	
70	40	78	-1.90E-01	-1.85E-01	-1.56E-01	-1.20E-01	2.69E-02	1.06E-02	2.55E-02	2.55E-02	-2.97E-02	2.55E-02	-2.97E-02	
		80	6.48E-02	-3.23E-01	2.80E-02	-2.66E-01	4.36E-03	2.81E-02	3.72E-02	3.72E-02	5.83E-03	3.72E-02	5.83E-03	
		82	3.77E-01	-1.65E-01	3.15E-01	-1.66E-01	-2.00E-02	1.77E-02	1.46E-02	1.46E-02	3.16E-02	1.46E-02	3.16E-02	
68	40	78	-1.88E-01	-1.87E-01	-1.54E-01	-1.26E-01	2.63E-02	1.06E-02	2.36E-02	2.36E-02	-2.87E-02	2.36E-02	-2.87E-02	
		80	6.63E-02	-3.23E-01	3.27E-02	-2.67E-01	4.17E-03	2.77E-02	3.57E-02	3.57E-02	4.91E-03	3.57E-02	4.91E-03	
		82	3.78E-01	-1.64E-01	3.18E-01	-1.63E-01	-1.99E-02	1.75E-02	1.46E-02	1.46E-02	3.02E-02	1.46E-02	3.02E-02	
66	40	78	-1.83E-01	-1.87E-01	-1.47E-01	-1.34E-01	2.50E-02	1.07E-02	2.02E-02	2.02E-02	-2.81E-02	2.02E-02	-2.81E-02	
		80	6.93E-02	-3.19E-01	4.10E-02	-2.65E-01	3.63E-03	2.71E-02	3.39E-02	3.39E-02	2.74E-03	3.39E-02	2.74E-03	
		82	3.77E-01	-1.60E-01	3.20E-01	-1.57E-01	-1.98E-02	1.71E-02	1.54E-02	1.54E-02	2.81E-02	1.54E-02	2.81E-02	
75	42	78	-1.89E-01	-1.85E-01	-1.54E-01	-1.17E-01	2.76E-02	1.06E-02	2.62E-02	2.62E-02	-3.08E-02	2.62E-02	-3.08E-02	
		80	6.49E-02	-3.22E-01	2.64E-02	-2.63E-02	4.55E-03	2.85E-02	3.82E-02	3.82E-02	5.82E-03	3.82E-02	5.82E-03	
		82	3.77E-01	-1.64E-01	3.13E-01	-1.66E-01	-2.03E-02	1.80E-02	1.51E-02	1.51E-02	3.22E-02	1.51E-02	3.22E-02	



Table 12. Reflection coefficients as a function of break points in the exponential profile,  $\beta = 0.3$ ,  $h_w = 72$ , frequency = 30 kHz (Concluded).

Upper Break Altitude (km)	Lower Break Altitude (km)	Angle of Incidence (deg)	<u>R11</u>			<u>R22</u>			<u>R21</u>			<u>R12</u>		
75	43	78	-1.89E-01	-1.85E-01	-1.54E-01	-1.17E-01	2.76E-02	1.06E-02	2.62E-02	2.62E-02	1.06E-02	-3.08E-02	2.62E-02	-3.08E-02
		80	6.49E-02	-3.23E-01	2.64E-02	-2.63E-01	4.56E-03	2.85E-02	3.82E-02	3.82E-02	2.85E-02	5.82E-03	3.82E-02	5.82E-03
		82	3.77E-01	-1.64E-01	3.13E-01	-1.66E-01	-2.03E-02	1.80E-02	1.51E-01	1.51E-01	1.80E-02	3.22E-02	1.51E-01	3.22E-02
75	44	78	-1.63E-01	-2.08E-01	-1.38E-01	-1.36E-01	2.60E-02	1.41E-02	3.00E-02	3.00E-02	1.41E-02	-2.72E-02	3.00E-02	-2.72E-02
		80	9.99E-02	-3.14E-01	5.51E-02	-2.59E-01	1.42E-03	2.89E-02	3.74E-02	3.74E-02	2.89E-02	9.95E-03	3.74E-02	9.95E-03
		82	3.90E-01	-1.31E-01	3.27E-01	-1.38E-01	-2.18E-02	1.62E-02	1.22E-02	1.22E-02	1.62E-02	3.35E-02	1.22E-02	3.35E-02
75	45	78	-1.35E-01	-2.28E-02	-1.18E-01	-1.53E-01	2.40E-02	1.74E-02	3.33E-02	3.33E-02	1.74E-02	-2.30E-02	3.33E-02	-2.30E-02
		80	1.34E-01	-3.01E-01	8.33E-02	-2.51E-01	-1.73E-03	2.89E-02	3.61E-02	3.61E-02	2.89E-02	1.40E-02	3.61E-02	1.40E-02
		82	4.01E-01	-9.66E-02	3.38E-01	-1.09E-01	-2.32E-02	1.43E-02	9.28E-03	9.28E-03	1.43E-02	3.44E-02	9.28E-03	3.44E-02
72	41	78	-1.89E-01	-1.85E-01	-1.55E-01	-1.18E-01	2.74E-02	1.06E-02	2.62E-02	2.62E-02	1.06E-02	-3.05E-02	2.62E-02	-3.05E-02
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72	42	78	-1.89E-01	-1.85E-01	-1.55E-01	-1.18E-01	2.74E-02	1.06E-02	2.62E-02	2.62E-02	1.06E-02	-3.05E-02	2.62E-02	-3.05E-02
		80	6.47E-02	-3.22E-01	2.65E-02	-2.64E-01	4.46E-03	2.84E-02	3.80E-02	3.80E-02	2.84E-02	5.92E-03	3.80E-02	5.92E-03
		82	3.76E-01	-1.65E-01	3.13E-01	-1.66E-01	-2.02E-02	1.79E-02	1.49E-02	1.49E-02	1.79E-02	3.22E-02	1.49E-02	3.22E-02

method selected for nighttime was to adjust the ambient value of  $Q$ , ( $Q_A$ ), at 95 km to match the exponential profile. This can be done while retaining a reasonable value for the production rate. Then for altitudes between 75 and 95 km the electron density is computed from

$$N_e = \exp (C_e' + x \ln Q)$$

where

$$C_e' = C_e \quad Q \geq 10 \cdot Q_A$$

$$C_e' = f_q C_x + (1 - f_q) C_e \quad Q < 10 \cdot Q_A$$

where

$$f_q = 1.11 - \frac{Q}{9Q_A} \quad \text{and}$$

$$Q_A = \text{normal (undisturbed) ion production rate (ion pairs/cm}^3\text{)}.$$

Note that  $f_q = 1$  ( $C_e' = C_x$ ) when  $Q = Q_A$  and  $f_q = 0$  ( $C_e' = C_e$ ) when  $Q = 10 Q_A$ .

The value  $C_x$  is the value of  $C_e$  required to reproduce the exponential electron density profile when  $Q = Q_A$ , ie,

$$C_x = \ln (N_e) - x \ln Q_A.$$

A similar procedure was used to fit the electron concentration profile over the altitude range from 40 to 75 km for daytime conditions, except that none of the normal values for  $Q_A$  were adjusted. This procedure is equivalent to an adjustment in atmospheric chemistry parameters, not production rate, and thus will not increase the sensitivity to weak disturbances. The model reproduces the original model data for  $Q$  greater than  $10 Q_A$ .

Figures 13 and 14 show the results produced by the simple model. Electron and positive ion concentrations are shown as a function of altitude, parametric in ion production rate produced by high-altitude spread debris. Uniformly spread debris is frequently used to characterize widespread VLF/LF disturbances. The spread debris parameter is

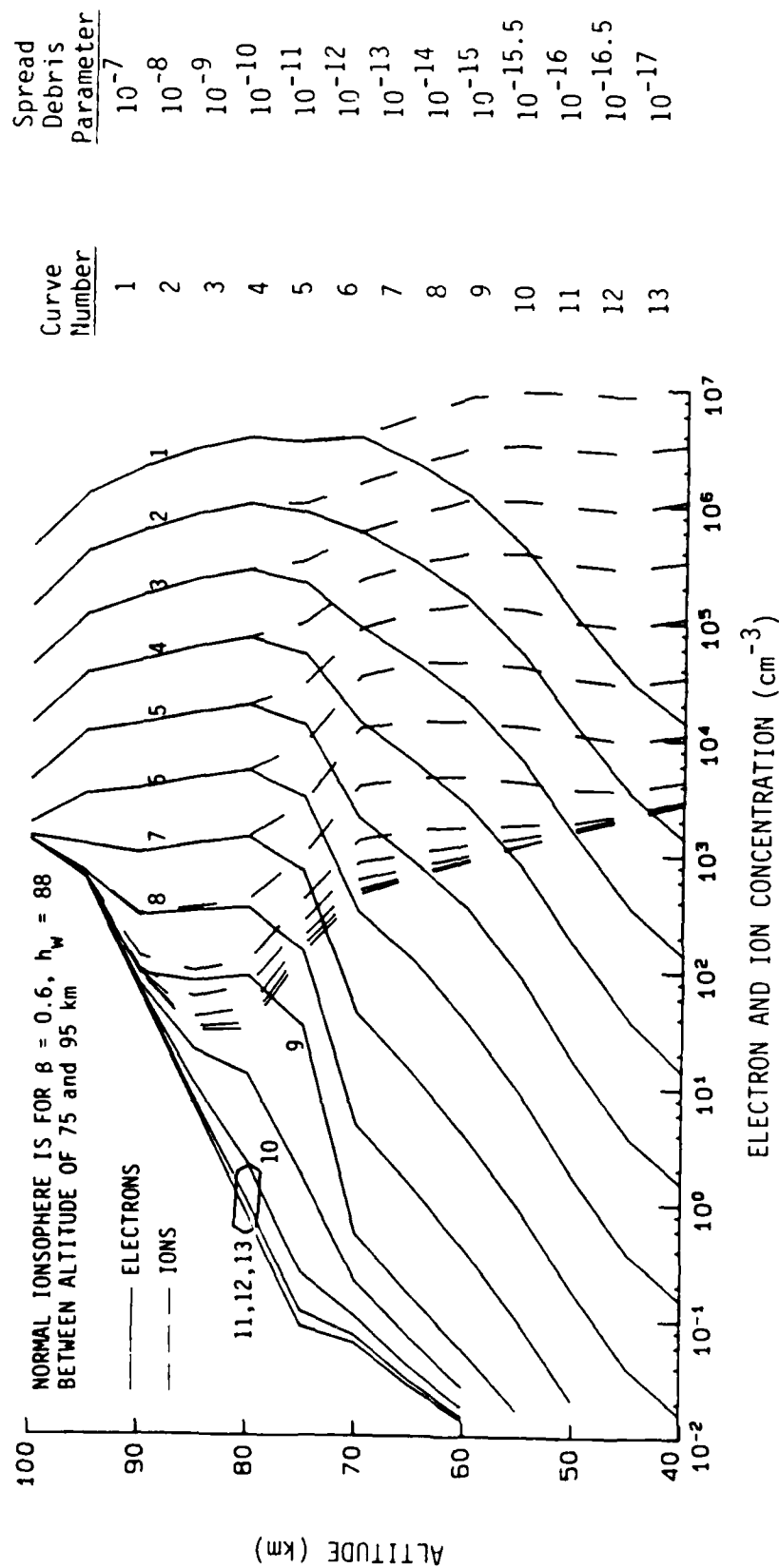


Figure 13. Electron and ion concentration produced by a spread debris source using the SIMBAL modified D-region ionization model (nighttime).

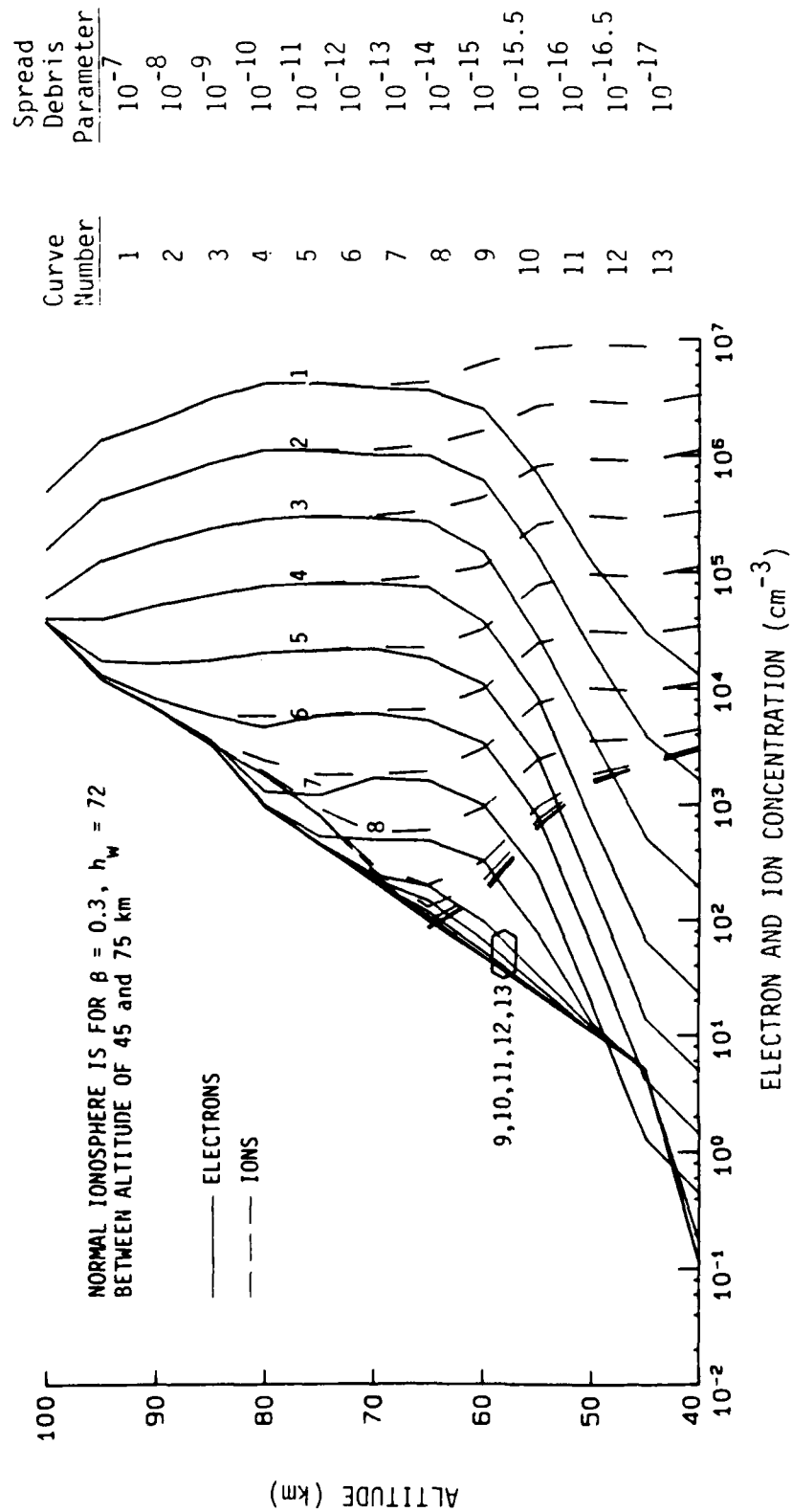


Figure 14. Electron and ion concentration produced by a spread debris source using the SIMBAL modified D-region ionization model (daytime).

$$w = \frac{W_F}{A_d t^{1.2}}$$

where

$W_F$  = fission yield (MT)

$A_d$  = area covered by the high-altitude debris cloud ( $\text{km}^2$ )

$t$  = time since detonation (sec).

Results are shown for a range of values of  $w$  from  $10^{-7}$  (a very intense disturbance) to a value of  $10^{-17}$  (smaller than the normal production rate for both nighttime and daytime conditions). The transition from the exponential for small disturbances is reasonably smooth.

The ion concentration is unchanged from the previous model. One has to be careful in adjusting (reducing) electron concentrations to be sure that the relative effect of ions is not unrealistically increased. The ion and electron concentration curves do not merge at higher altitudes as they should. However, the ion concentration predicted by the model for low  $Q$  will not have a significant effect on VLF/LF propagation.

### 3.4 REACTION RATE AND IONIZATION RATE ADJUSTMENT IN THE WEDCOM CHEMISTRY MODEL.

The lumped parameter chemistry model was briefly described in Section 1. The four lumped-parameter reaction rates (attachment rate,  $A$ , detachment rate,  $D$ , the ion-ion recombination coefficient,  $\alpha_i$ , and the electron-ion recombination coefficient,  $\alpha_d$ ) are computed using weighted average reactions between several atomic and molecular species in the atmosphere. The species are in equilibrium for a specified normal temperature profile. Arbitrary adjustment of the lumped parameters is similar to the numerical procedure described in Section 3-3. A realistic adjustment requires adjustment of atmospheric species, and changes for one application can cause unwanted changes to the model for other applications. In addition to the complications of adjusting the normal chemistry values, the atmospheric species and the associated reactions are affected by high levels of weapon-produced energy deposition. The weapon-induced changes can be long lasting; thus changes to match preburst conditions do not guarantee recovery to preburst conditions for long periods of time.

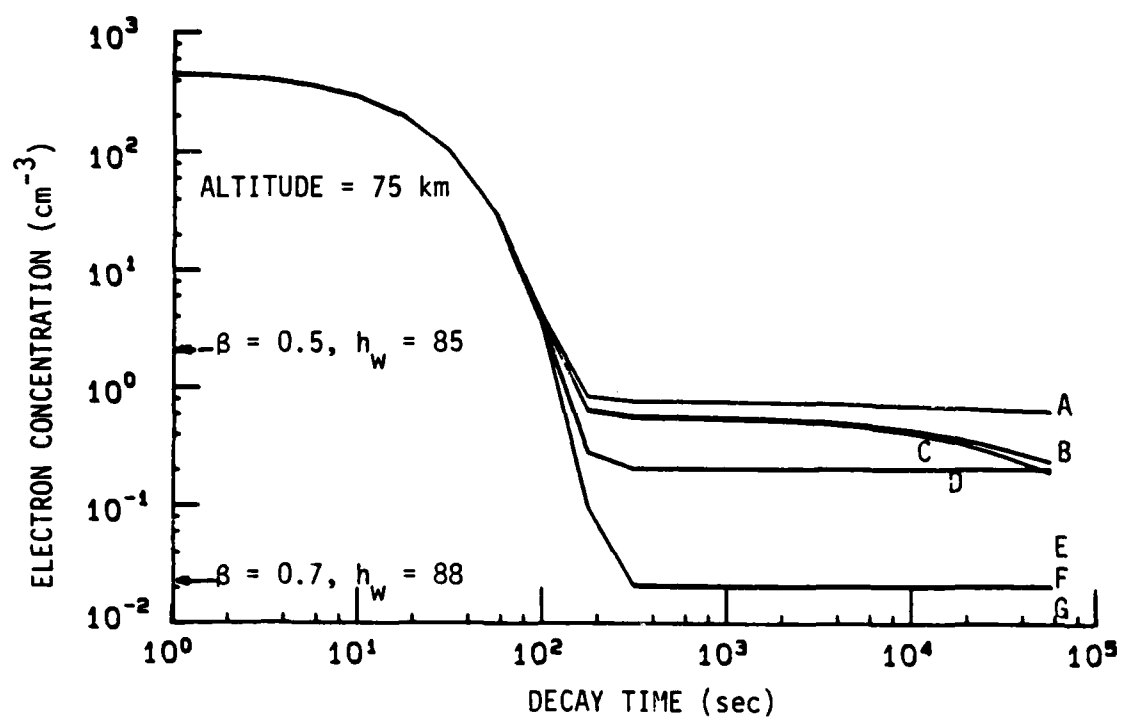
The effort described here is not an effort to modify the complex chemistry model. It is a numerical or sensitivity study to indicate the range of values the lumped parameters and ionization rates must have to produce specified profiles.

Emphasis here is placed on nighttime conditions, where the requirement to match propagation data requires reduction of model electron concentration in the 75 to 95 km altitude range. There is a lower limit that can be achieved by simply reducing the ion production rate. This limit is imposed by the maximum decay from realistic daytime values. While any level of quasi-equilibrium electron density can eventually be attained, the actual midnight values are determined by the maximum decay in about a twelve-hour period from daytime conditions. The logical chemistry parameter to vary (Reference 17) is the detachment rate, since the detachment rate varies several orders of magnitude in the altitude range of interest. A change in the altitude distribution of important species (in this case atomic oxygen) can produce orders of magnitude changes in the detachment rate at a specified altitude. (Changes in both attachment and detachment rates which result in the same change in the ratio of A to D would produce results roughly equivalent to those obtained by changing D alone).

Several parametric calculations were performed to test the sensitivity of nighttime electron concentration profiles to changes in Q and D. The calculations were performed in a way to produce a lower limit to the estimated values of nighttime electron values. The procedure was as follows:

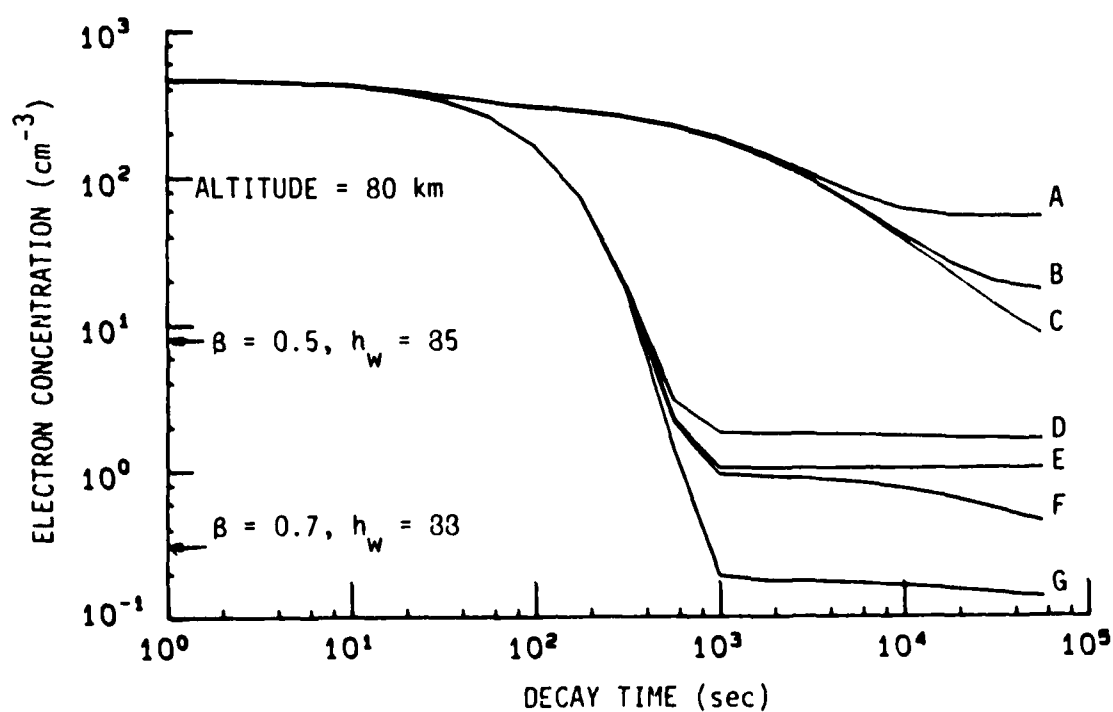
1. Set the initial electron and positive ion concentration values to normal noontime values.
2. Assume that the ambient  $Q(Q_a)$  and reaction rates are the midnight values.
3. Compute the electron concentration as a function of time.
4. Modify the  $Q_a$ 's and the detachment rate and repeat 1 through 3.

The calculations were made using Subroutine DTNE (Reference 18) which performs a transient electron concentration calculation for fixed reaction rates. Results were obtained for altitudes of 75, 80, 85, and 90 km and are shown in Figures 15 through 18. The curves all have the same characteristic shape, consistent with the approximate relations in Reference 19 which show the decay from an initial value for no production rate. The electron density quickly decays from the noontime value with an exponential decay according to



Curve	Ion Production Rate	Detachment Rate
A	$10^{-2}$	$5.76 \times 10^{-5}$
B	$10^{-3}$	$5.76 \times 10^{-5}$
C	$10^{-4}$	$5.76 \times 10^{-5}$
D	$10^{-2}$	$5.76 \times 10^{-8}$
E	$10^{-2}$	$5.76 \times 10^{-9}$
F	$10^{-3}$	$5.76 \times 10^{-8}$
G	$10^{-3}$	$5.76 \times 10^{-9}$

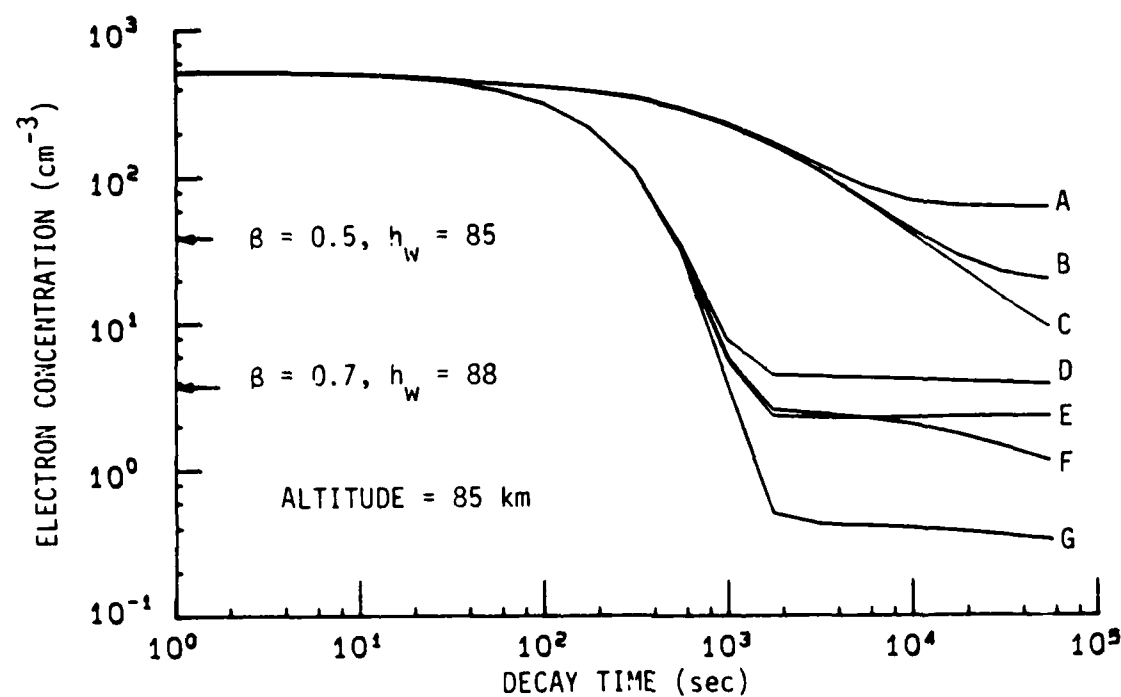
Figure 15. Electron decay from noontime conditions at 75 km altitude.



Curve	Ion Production Rate	Detachment Rate
A	$10^{-2}$	$1.93 \times 10^{-2}$
B	$10^{-3}$	$1.93 \times 10^{-2}$
C	$10^{-4}$	$1.93 \times 10^{-2}$
D	$10^{-2}$	$1.93 \times 10^{-5}$
E	$10^{-2}$	$1.93 \times 10^{-6}$
F	$10^{-3}$	$1.93 \times 10^{-5}$
G	$10^{-3}$	$1.93 \times 10^{-6}$

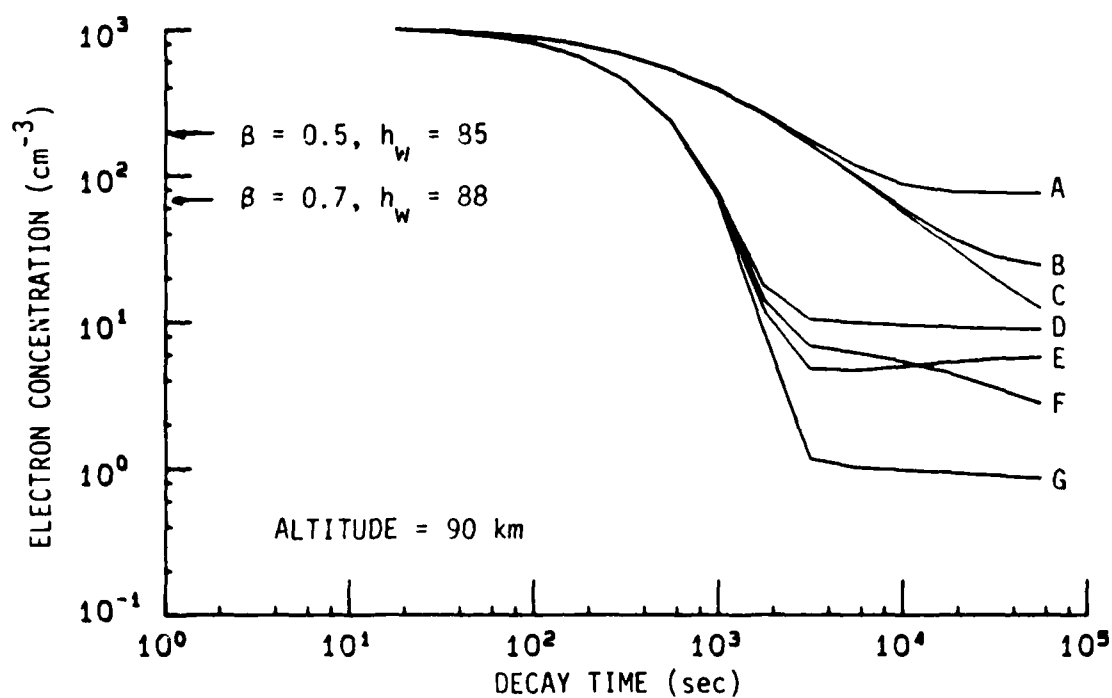
Figure 16. Electron decay from noontime conditions at 80 km altitude.





Curve	Ion Production Rate	Detachment Rate
A	$10^{-2}$	$2.39 \times 10^{-2}$
B	$10^{-3}$	$2.39 \times 10^{-2}$
C	$10^{-4}$	$2.39 \times 10^{-2}$
D	$10^{-2}$	$2.39 \times 10^{-5}$
E	$10^{-2}$	$2.39 \times 10^{-6}$
F	$10^{-3}$	$2.39 \times 10^{-5}$
G	$10^{-3}$	$2.39 \times 10^{-6}$

Figure 17. Electron decay from noontime conditions at 85 km altitude.



Curve	Ion Production Rate	Detachment Rate
A	$10^{-2}$	$2.16 \times 10^{-2}$
B	$10^{-3}$	$2.16 \times 10^{-2}$
C	$10^{-4}$	$2.16 \times 10^{-2}$
D	$10^{-2}$	$2.16 \times 10^{-5}$
E	$10^{-2}$	$2.16 \times 10^{-6}$
F	$10^{-3}$	$2.16 \times 10^{-5}$
G	$10^{-3}$	$2.16 \times 10^{-6}$

Figure 18. Electron decay from noontime conditions at 90 km altitude.

$$N_e(t) \propto e^{-(A+D)t}$$

The fast decay continues until

$$N_e(t) \approx \frac{D}{A+D} \frac{N_i}{1 + \alpha N_i t},$$

where  $N_i$  is the initial value, after which the decay is much slower. Note that the effect of very small ionization rates has no effect until decay time is in excess of 10,000 seconds.

Also shown on the curves for reference are the values of electron concentration that would be computed for the given altitude using exponential profiles with specified values of  $\beta$  and  $h_w$ . It can be seen that reducing the value of  $Q$  below the nominal values has little effect and that reduction in the detachment rate by a factor of 1000 to 10,000 is required to achieve the electron values for  $\beta = 0.7$ ,  $h_w = 88$  at altitudes of 75 and 80 km. At 85 km the reduction required for  $D$  is 100 to 1000 and at 90 km no reduction is required.

Figure 19 shows a plot of the WECOM winter-midnight reaction rates. The rapid variation of  $D$  in the altitude range of interest is apparent. The dashed curves bracket the values of  $D$  required to produce values of electron concentration consistent with the exponential profile with  $\beta = 0.7$  and  $h_w = 88$ . An adjustment in the fraction of atomic oxygen dissociated in the altitude range between 75 and 90 km altitude could produce the change in  $D$  (Reference 17). Another mechanism that could be involved is the existence of minor species that dominate the reactions at low ionization levels.

The consistency of such a modification with uncertainties in the model and its impact on other model features requires examination beyond the scope of this effort. Another question is whether such a change, if implemented, should apply for low or all ionization rates. The results do identify a possible model variation that would allow WEDCOM users to choose ionospheric profiles to match selected preburst conditions.

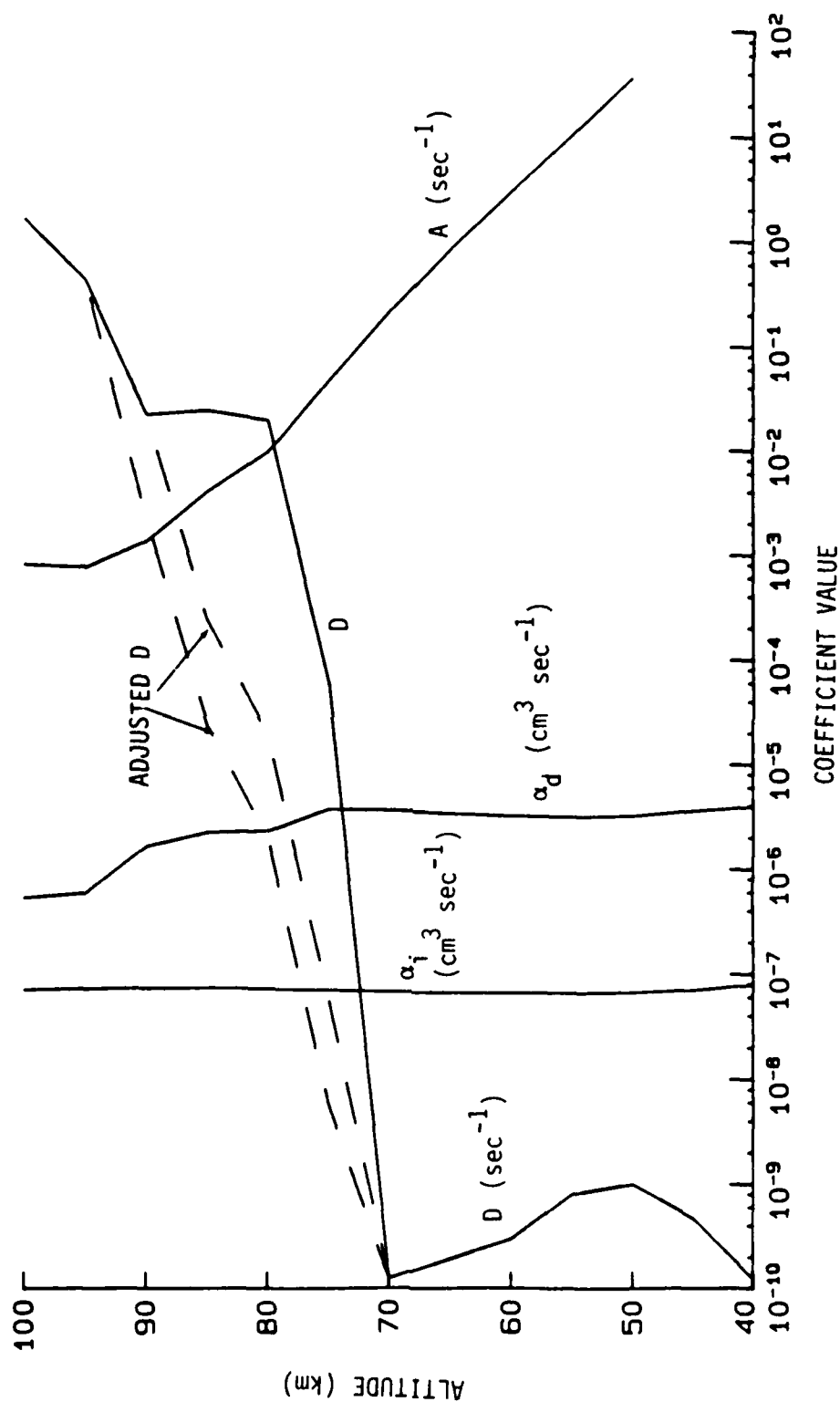


Figure 19. WECOM reaction rates for winter night.

SECTION 4  
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